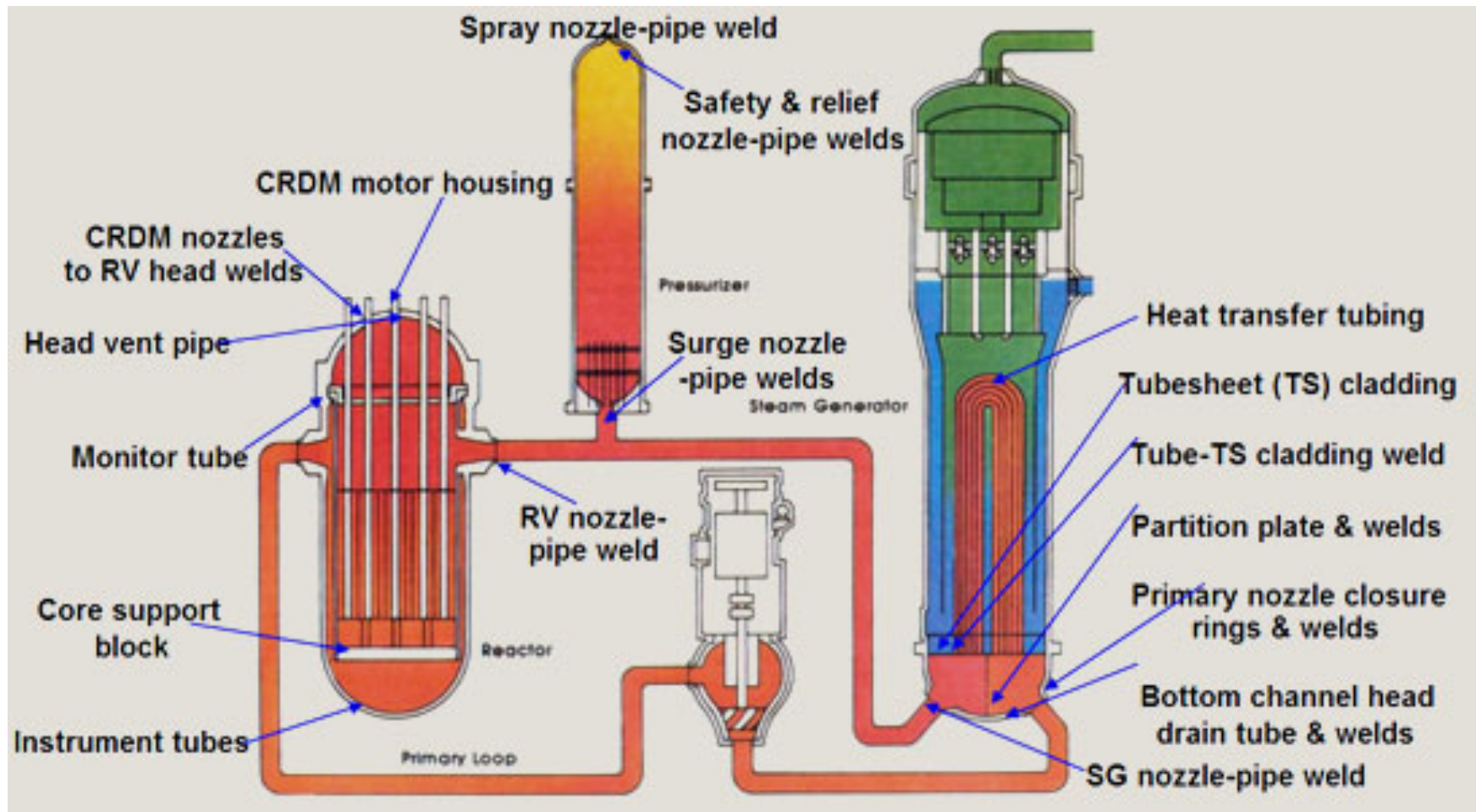




# Validating 3D two-parameter fracture mechanics for structural integrity assessments

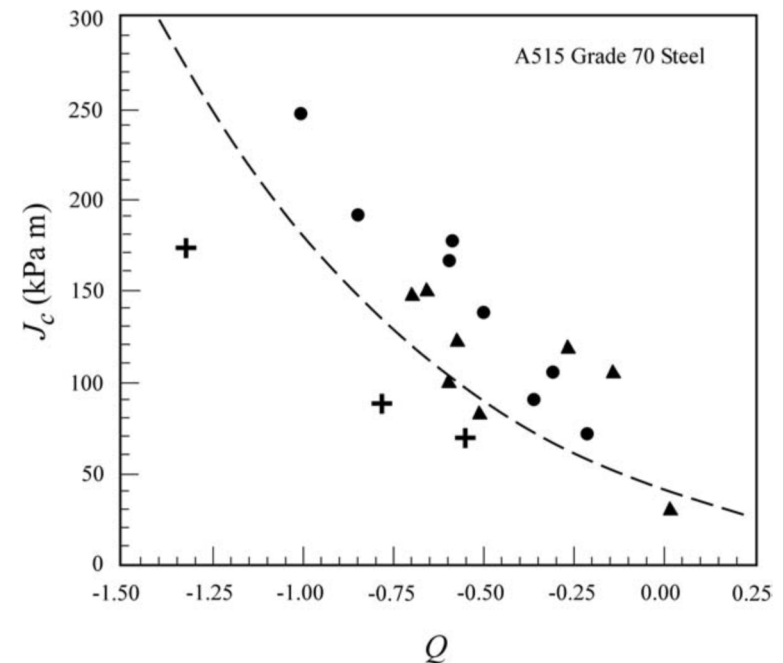
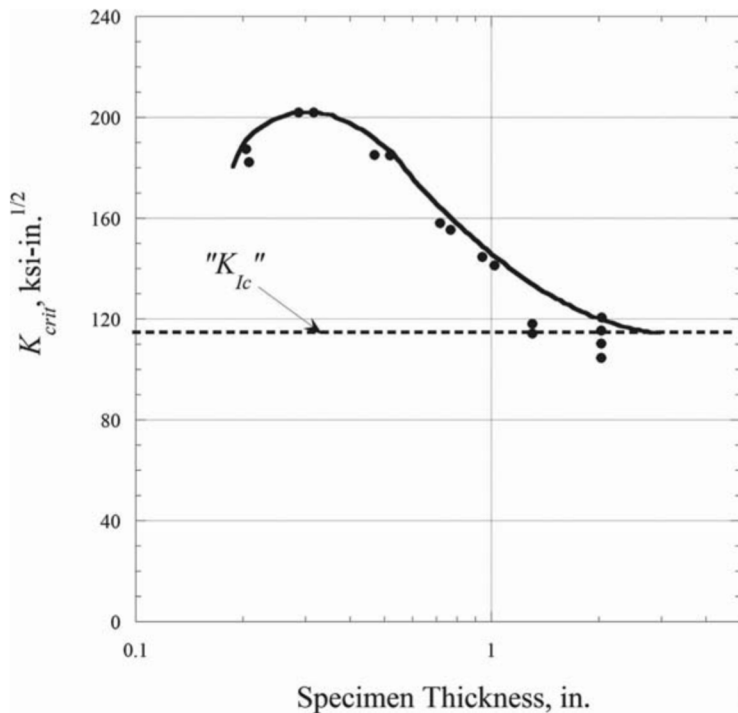
C. A. Simpson, S. Tonge, A. Cinar,  
C. Reinhard, T. J. Marrow, M.  
Mostafavi

# 🔥 Why do we do this?



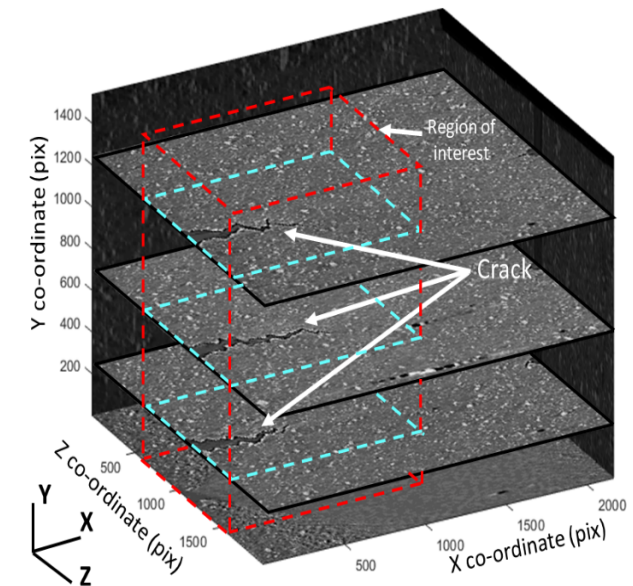
## 🔥 How do we test against fracture?

- » Long crack
- » Thick sample
- » Minimum fracture energy



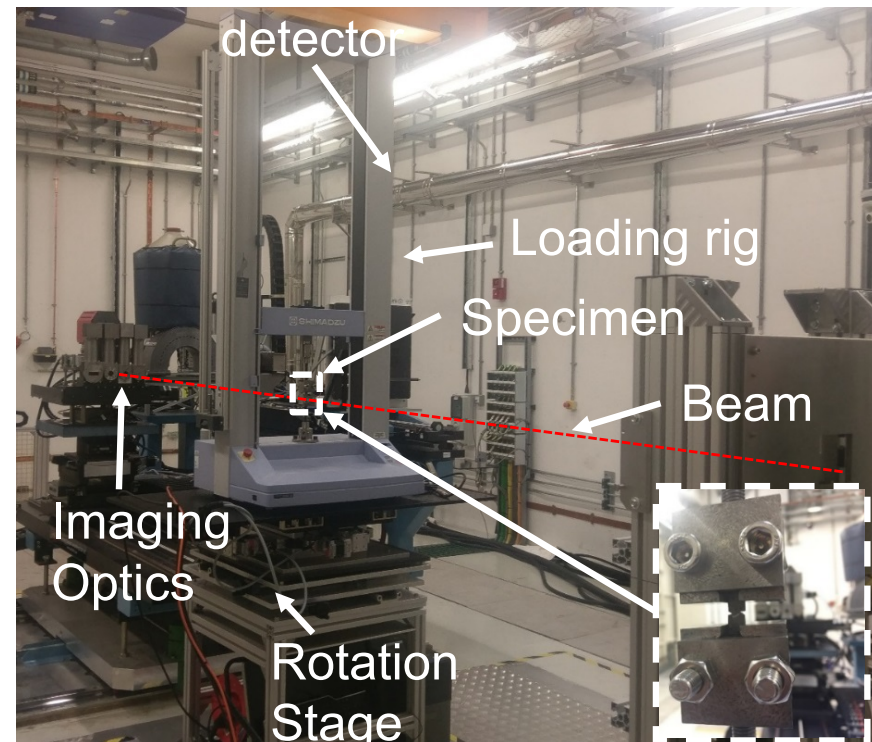
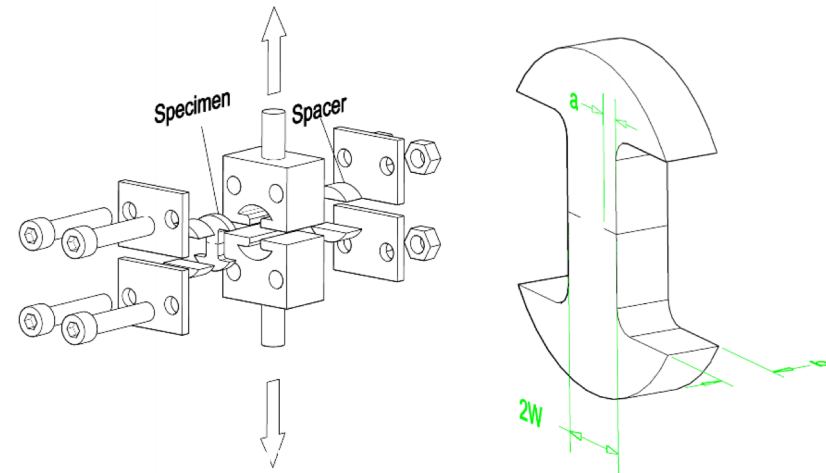
## 🔥 What was our aim?

- » In structural integrity assessment, we talk about T, Q (in-plane) and Tz (out-of-plane).
  - *Either* in-plane or out-of-plane constraint
- » New approaches are being developed that assess the amount of plasticity around the crack-tip.
  - More understanding and validation is still needed!
- » Aim to develop that understanding and provide additional, fundamental detail to underpin these calculations
  - Find plastic zone.
  - Separate  $J_{\text{total}}$  into plastic/elastic component
  - Through thickness variation in J



## Experiment Overview

- » Al-Ti Double-edge notch tension samples (DENT)
- » Varying the amount of 2D plastic constraint
  - $a/W = 0.1, 0.5$
  - $b = 5\text{mm}, 20\text{mm}$
  - *One combination covered here*
- » Work carried out at the DLS
  - I12:JEEP beamline
- » 2 part experiment
  - Monochromatic XRD (elastic)
  - XCT/DVC (elastic + plastic)



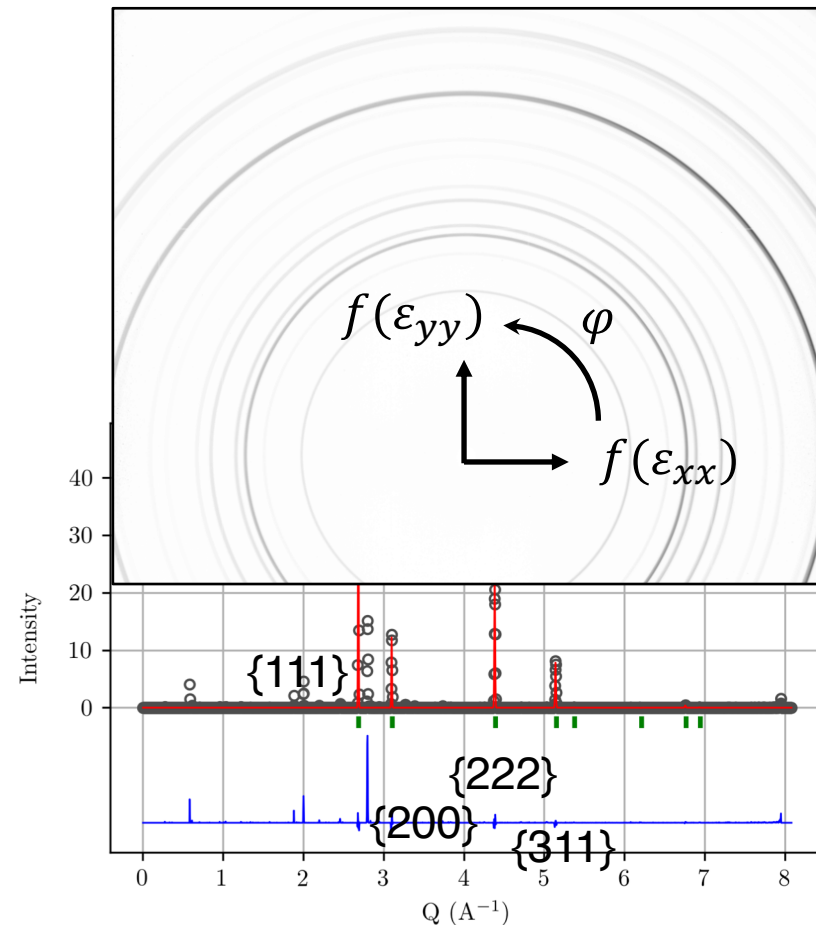
## 🔥 X-ray Diffraction (XRD)

### » Monochromatic 2D diffraction

- Energy = 60 keV
- Caking:  $\Delta\varphi = 10^\circ$
- $d$ ,  $a$  calculated according to Bragg's Law:
- $\varepsilon = \Delta d/d_0$

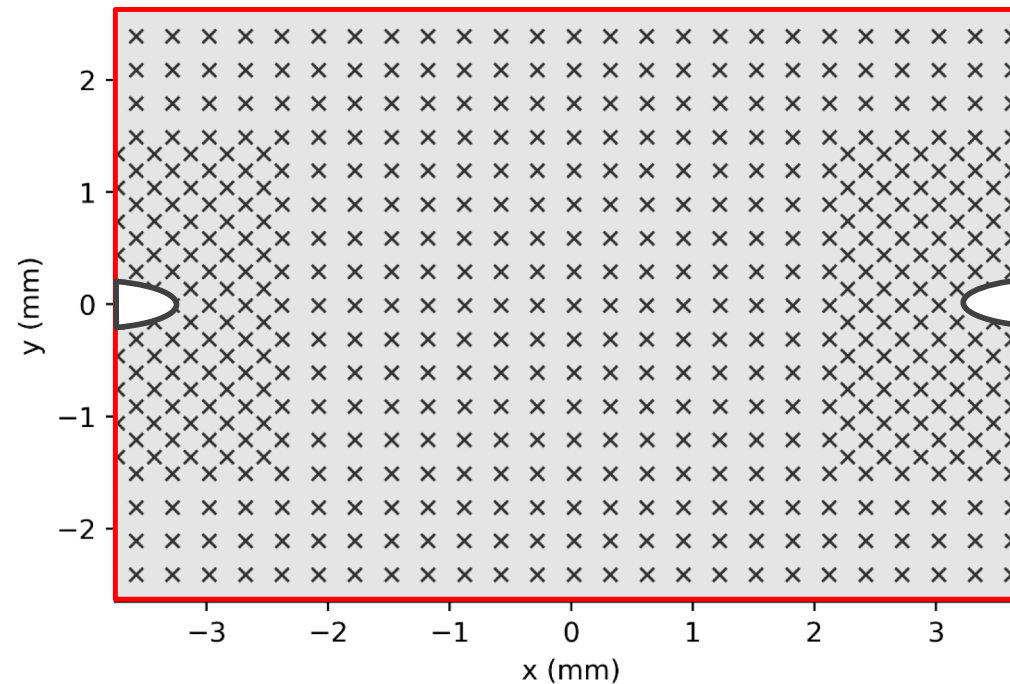
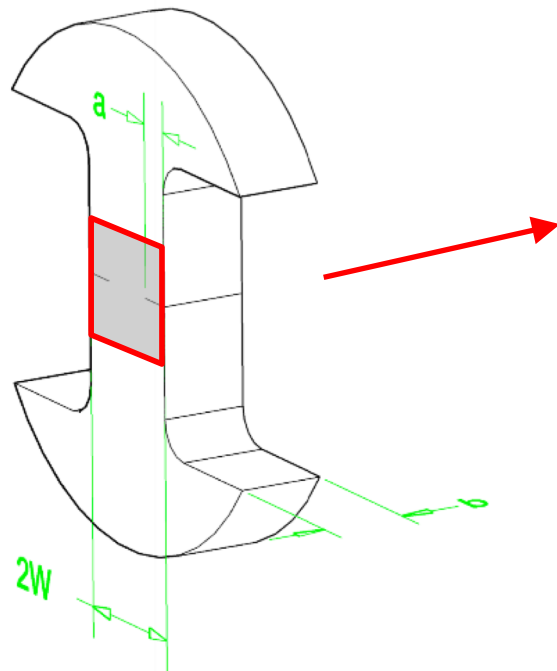
» 600 measurements made across a 2D grid...

» Looking to quantify 2D elastic strain and  $J_{\text{elastic}}$



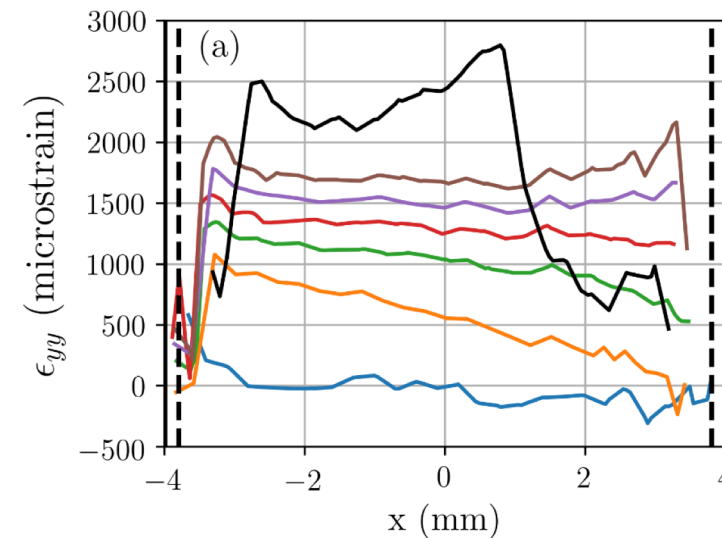
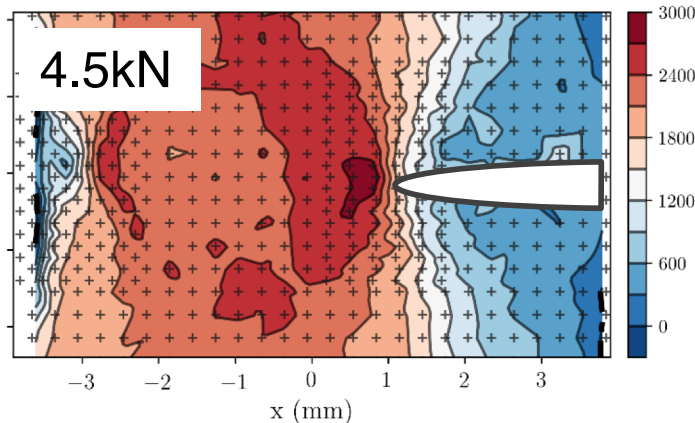
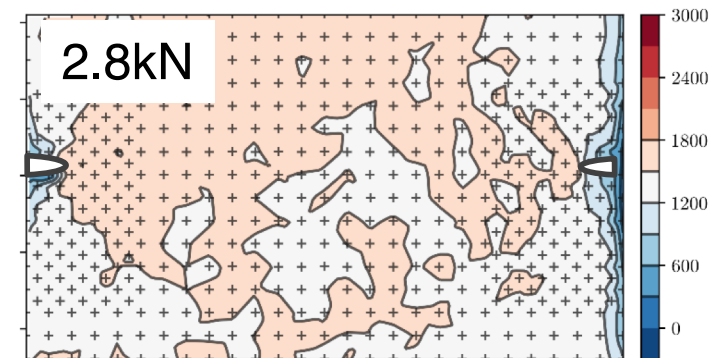
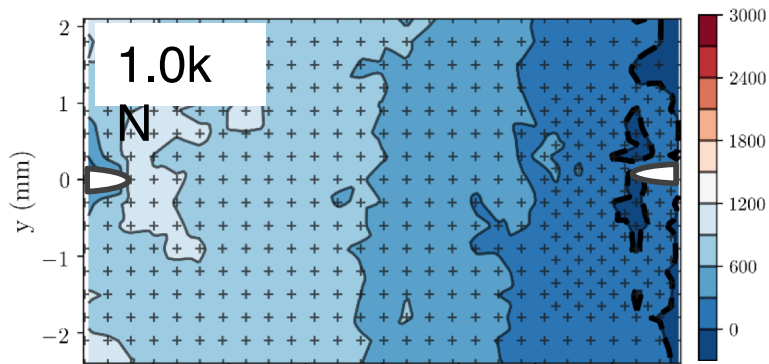


## 2D XRD Strain Maps



- » Approx. 600 points in total
- » High point density at around notch (high strain gradient)

## 🔥 2D XRD Strain Maps ( $\epsilon_{yy}$ ): $b = 5\text{mm}$ , $a/W = 0.1$



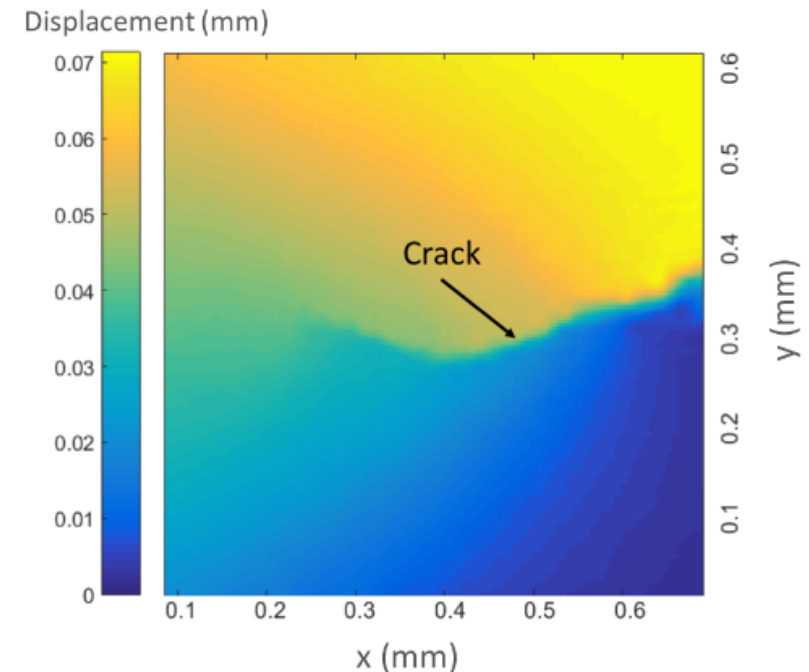
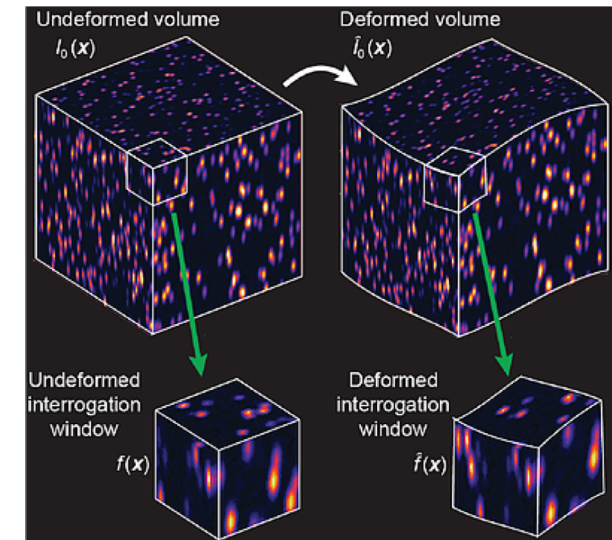
» Next step -> use 2D elastic strain to calculate  $J_{\text{elastic}}$  [1]

[1] Barhli, S. M. e al. (2016). Obtaining the J-integral by diffraction-based crack-field strain mapping. *Procedia Structural Integrity*, 2, 2519–2526.



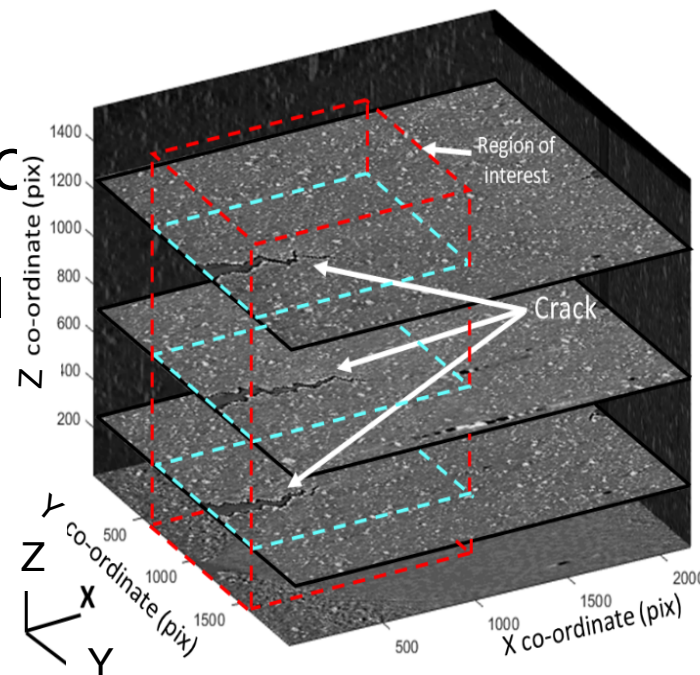
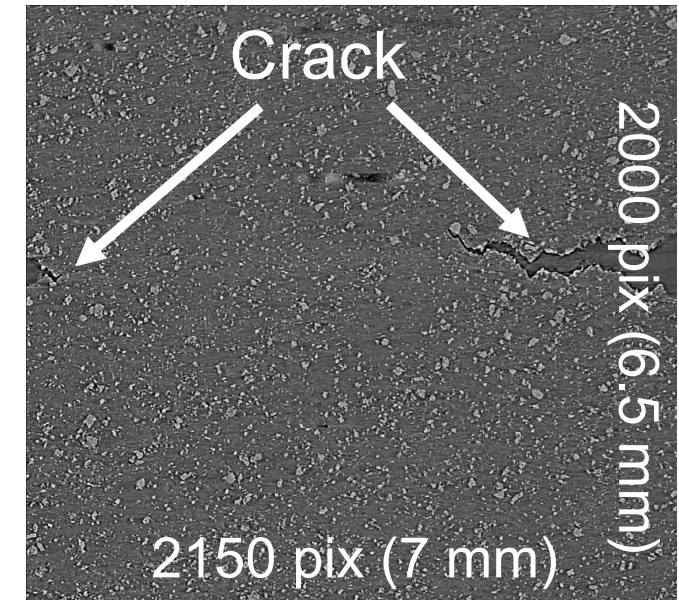
## Digital Volume Correlation

- » 3D equivalent to digital image correlation
- » Used to determine displacement and strain fields in 3D volumes
- » Tomogram is divided into overlapping sub-volumes
  - Sub-volume size of 16 voxels
  - 80% Overlap

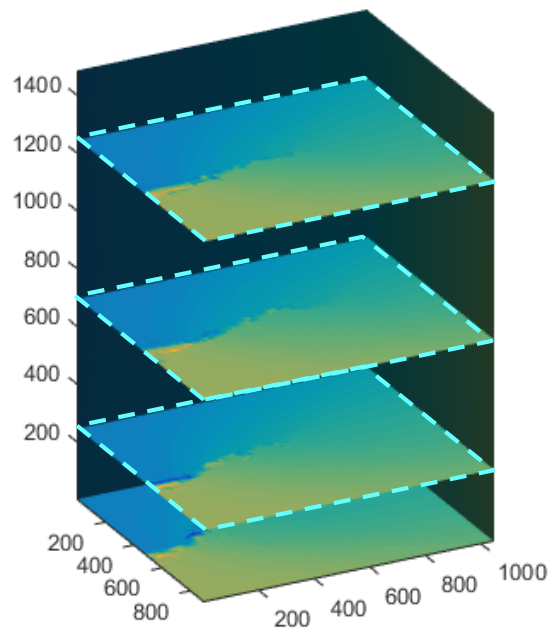


🔥 X-ray CT:  $b = 5\text{mm}$ ,  $a/W = 0.1$

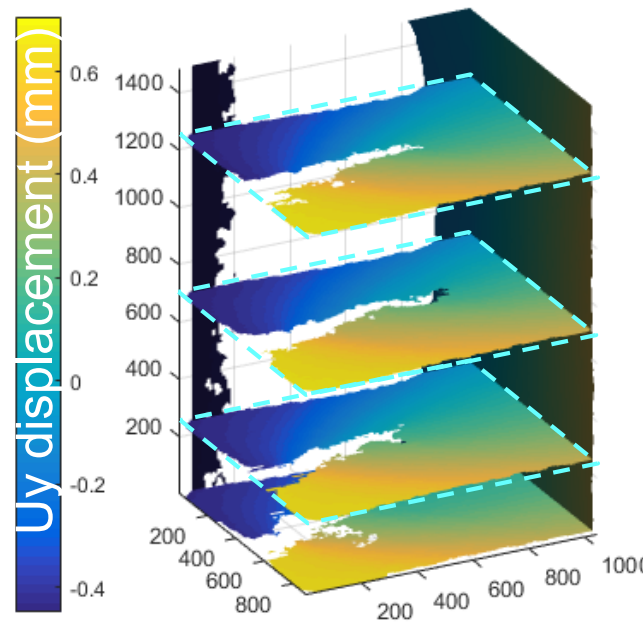
- » Limited angle X-ray computed tomography
  - $145^\circ$
  - 60 keV, 2501 projections
  - Voxel size  $\sim 4\mu\text{m}$
- » Al-Ti selected for its inherent speckle
  - Provides contrast for DVC
- » Aim is to evaluate COD, total strain and  $J_{\text{total}}$



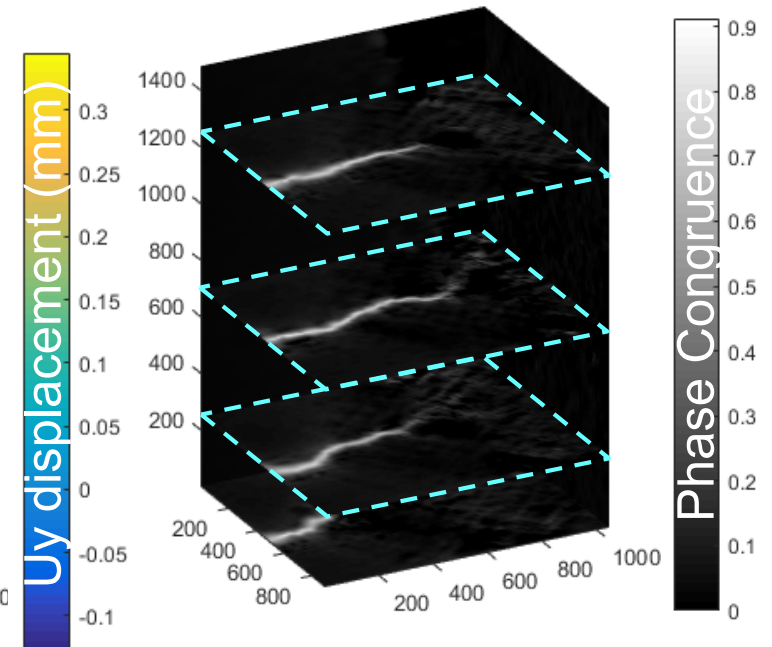
## 🔥 DVC/Phase Congruency Workflow



**Raw Uy  
displacement**



**Outlier  
deletion and  
extrapolation**

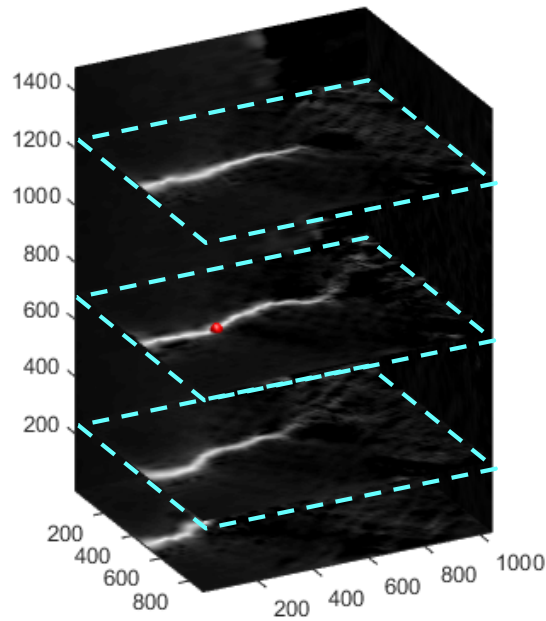


**Volumetric  
Phase  
congruency**

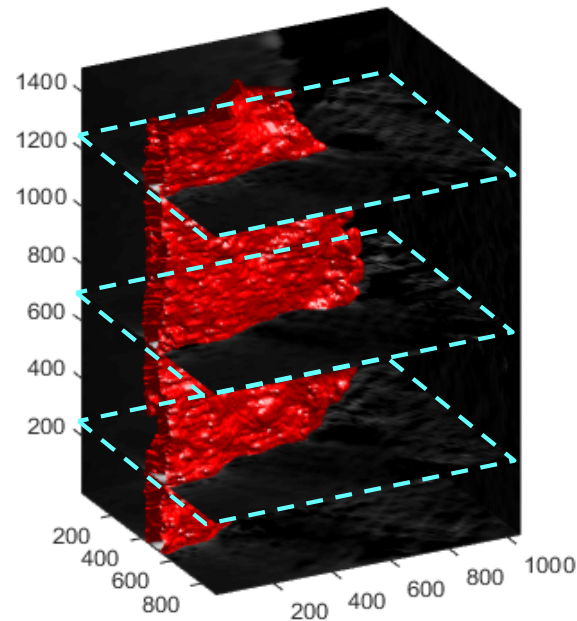
[1]

*Cinar, A. F. et al. (2017). An autonomous surface discontinuity detection and quantification method by digital image correlation and phase congruency. Optics and Lasers in Engineering, 96, 94–106.*

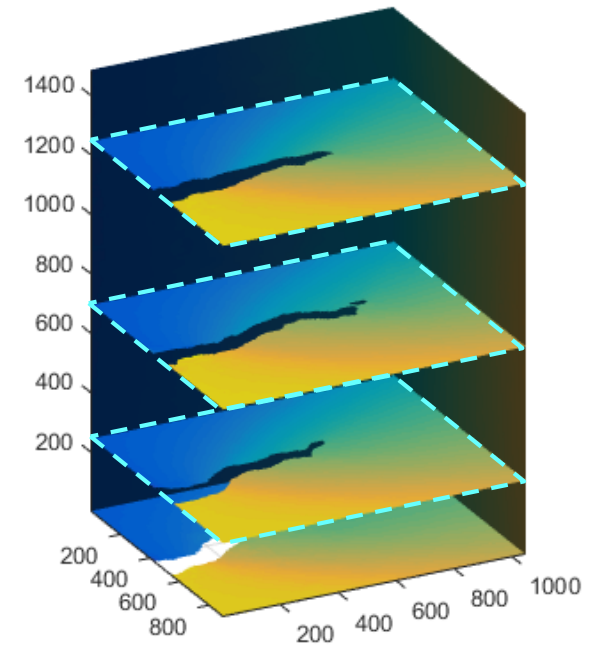
# Crack Segmentation Workflow



**Seeding point  
Selection**



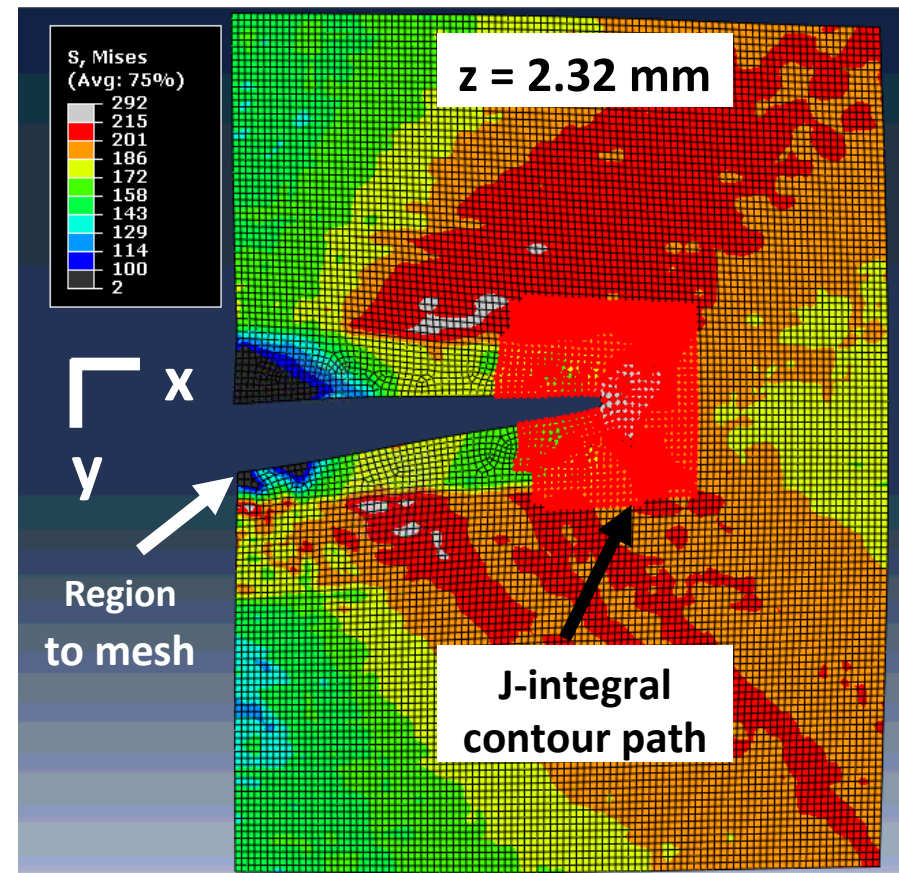
**Segmentation**



**Segmentation  
boundary  
identification**

## 🔥 J-integral Calculation (OUR-OMA)

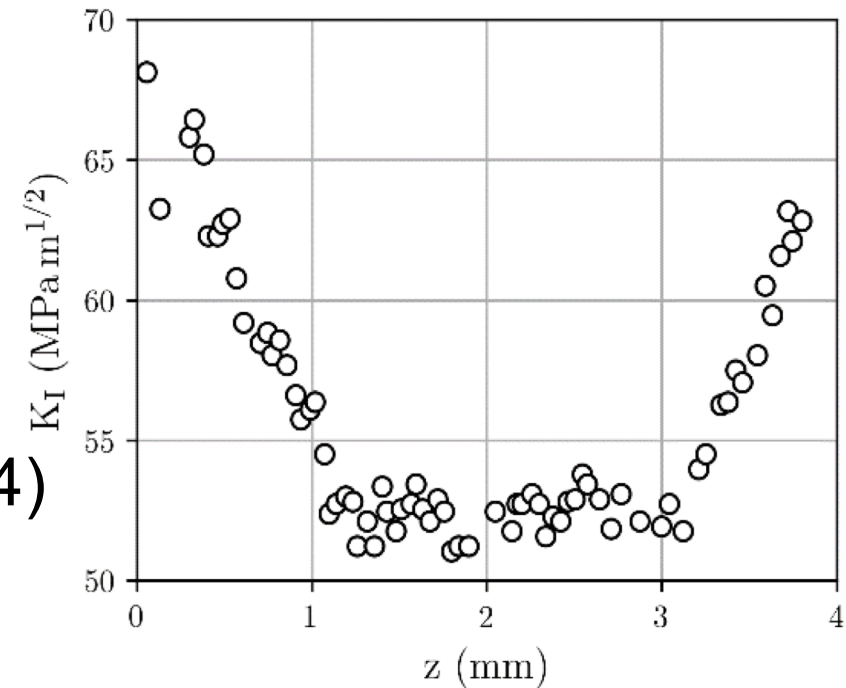
- » Import displacement fields into Abaqus
- » Segment crack path (using VPC-CD derived values)
- » Automatic FE meshing of region around crack path
- » Contour integral around crack evaluated by FE solver (domain integral method)



Barhli, S. M. et al. (2017). J-Integral Calculation by Finite Element Processing of Measured Full-Field Surface Displacements. *Experimental Mechanics*, 57(6), 997–1009.

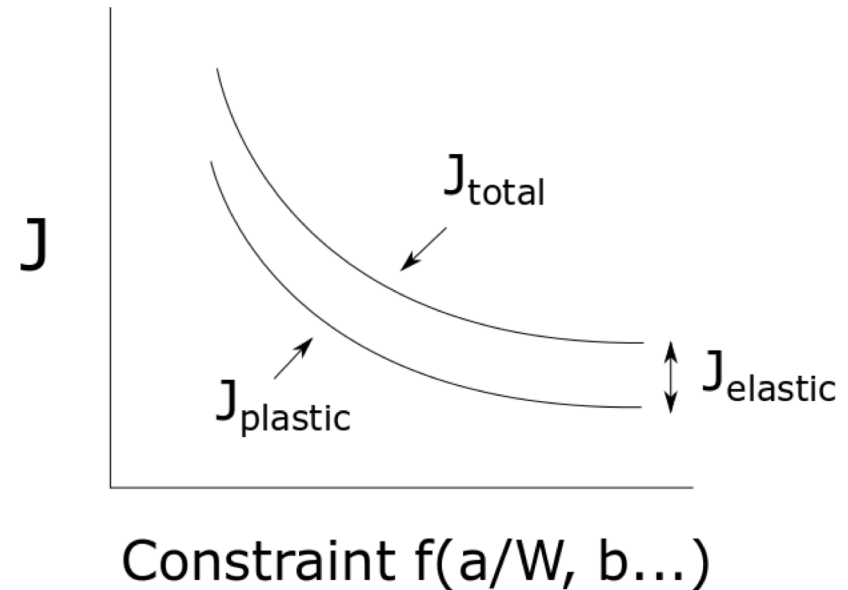
## Initial Results - $J_{\text{total}}$

- »  $J_{\text{total}}$  converted to  $K$ :
  - $K_I = \sqrt{J E}$
- » Minimum value of  $52 \text{MPa m}^{1/2}$  reached at the sample centre
- » Results not in agreement with analysis by Petit and Dodds (2004)
  - Increased plasticity at sample surface?
  - Error in 2D slice-by-slice approach?



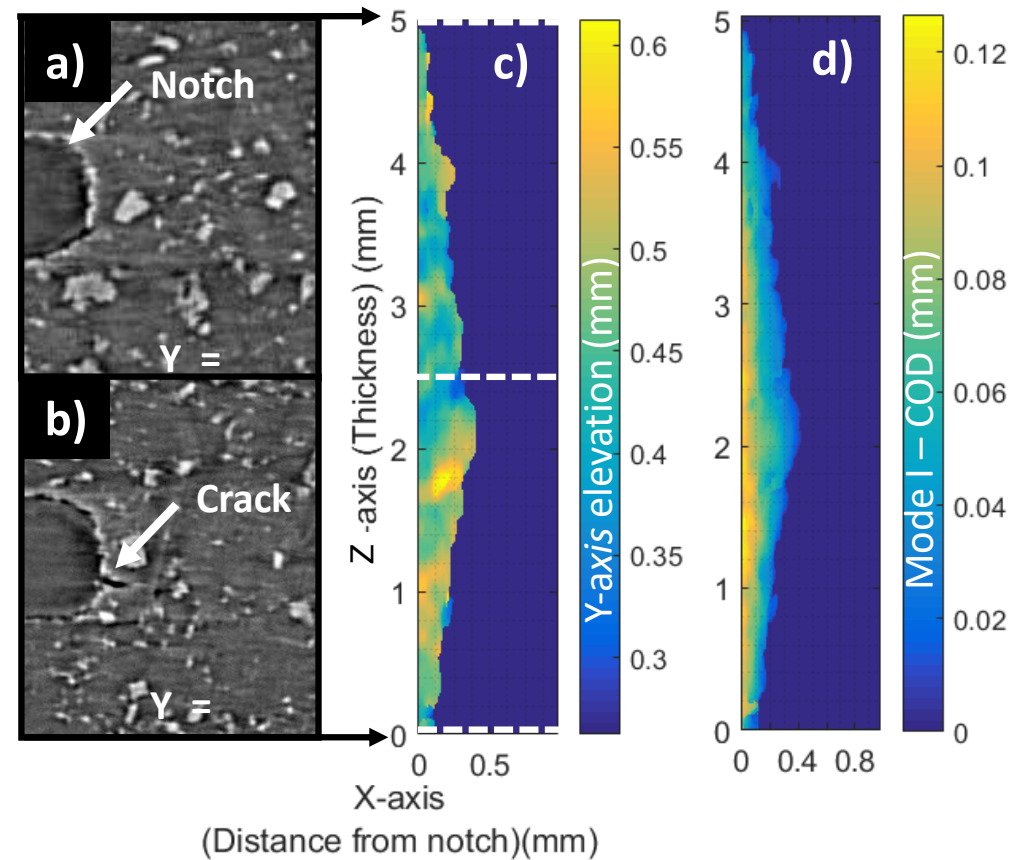
## 🔥 Conclusions and Where Next?

- » Sophisticated set of tools developed to tackle this problem
  1. VPC-CD (crack detection)
  2. OUR-OMA (J from DVC)
  3. JMAN-S (J from XRD strain)
  4. pyXe (XRD analysis)
  
- » Efforts are beginning to yield quantitative information!
  
- » Next steps are to:
  1. Calculate  $J_{\text{elastic}}$  from code (JMAN-S)
  2. Separate of  $J_{\text{elastic}}$  and  $J_{\text{plastic}}$  from  $J_{\text{total}}$
  3. Look at the variation in  $J_{\text{elastic}}$  wrt 2D plastic constraint
    - ***Does this remain constant?***



## 🔥 Crack Opening Displacement (COD)

- » Thin sample, long notch
  - $B = 5\text{mm}$ ,  $a/W = 0.1$
- » Through thickness crack elevation (crack tortuosity)
  - Interesting to capture the 3D crack path!
- » Associated crack opening displacements wrt. through thickness position also interrogated.





## 🔥 Conclusions

- » Image based damage mechanics can help calculate parameter that were not measurable before
- » Combination of 3D finite element and digital volume correlation can provide accurate boundary conditions
- » DVC and XRD can be used to separate elastic and plastic strains
- » Work of fracture through the thickness of specimens was calculated in this work