



Micromechanics of fibrous composites and permeability of fibrous media based on micro-CT images

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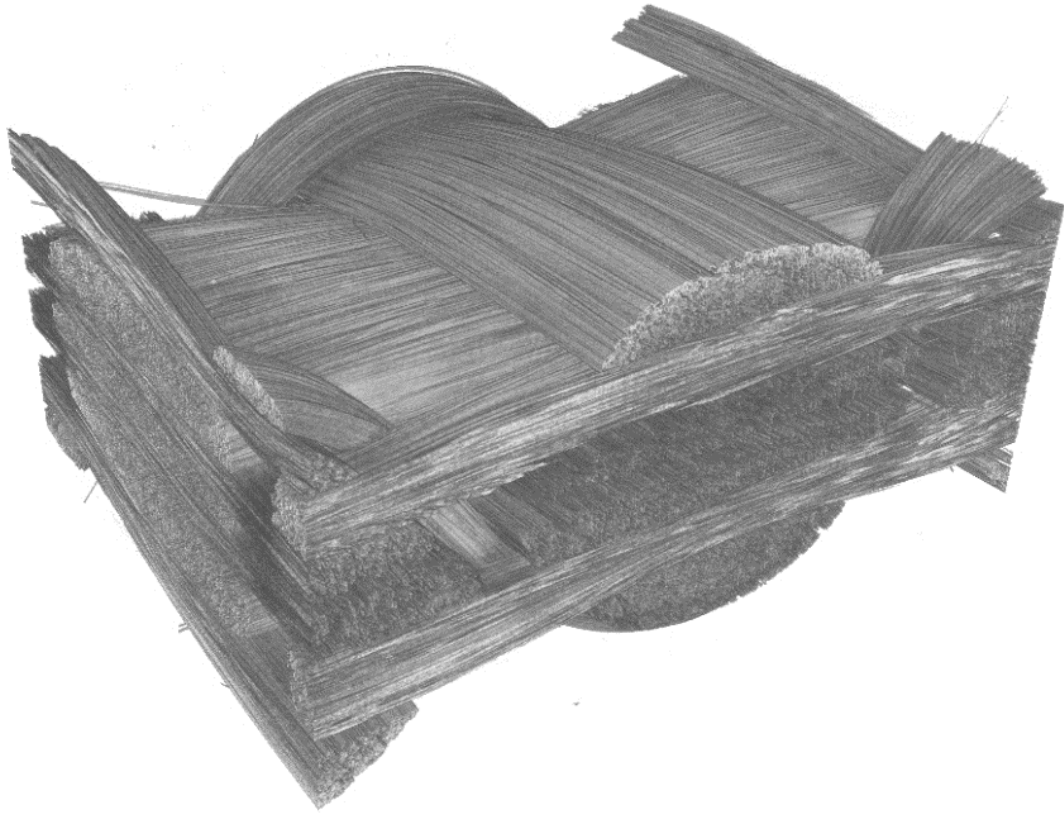
Through the μ CT and what we found there

1. Introduction. Fibrous media: microstructural features and characteristics
2. Quantification of a μ CT image of fibrous materials
3. Applications
 - Fibre orientations
 - Finite element models of deformation and damage
 - Permeability
4. Conclusions

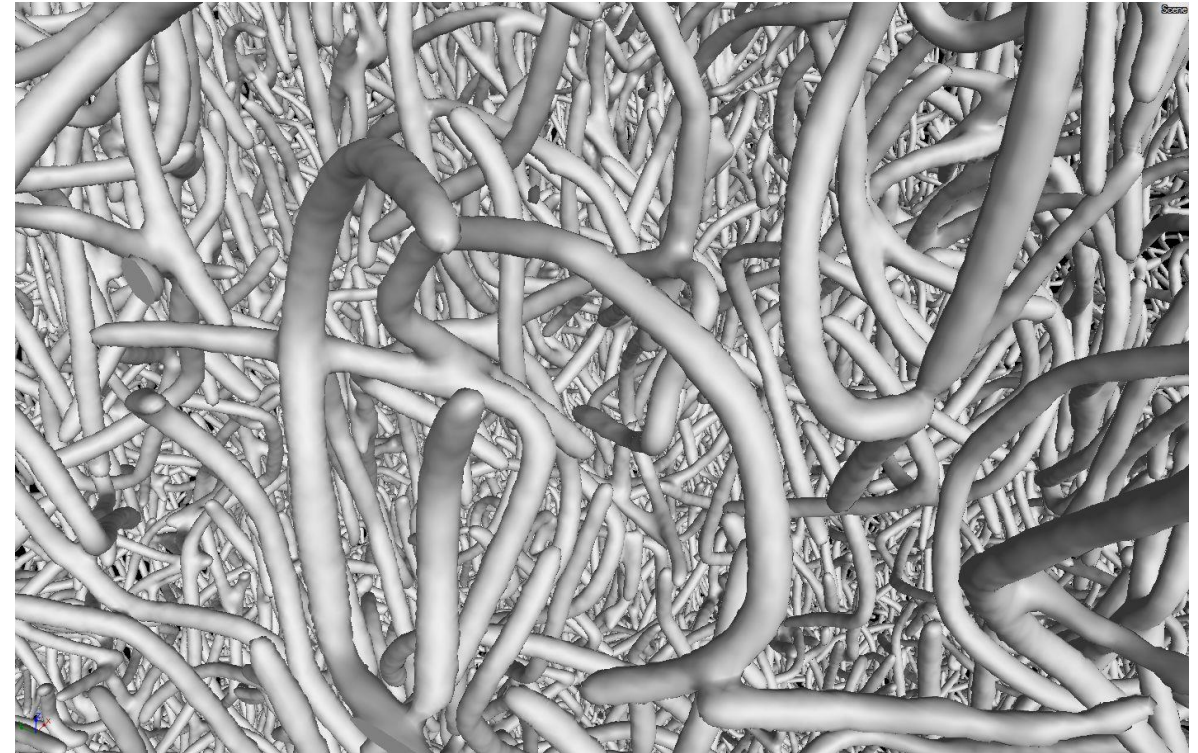


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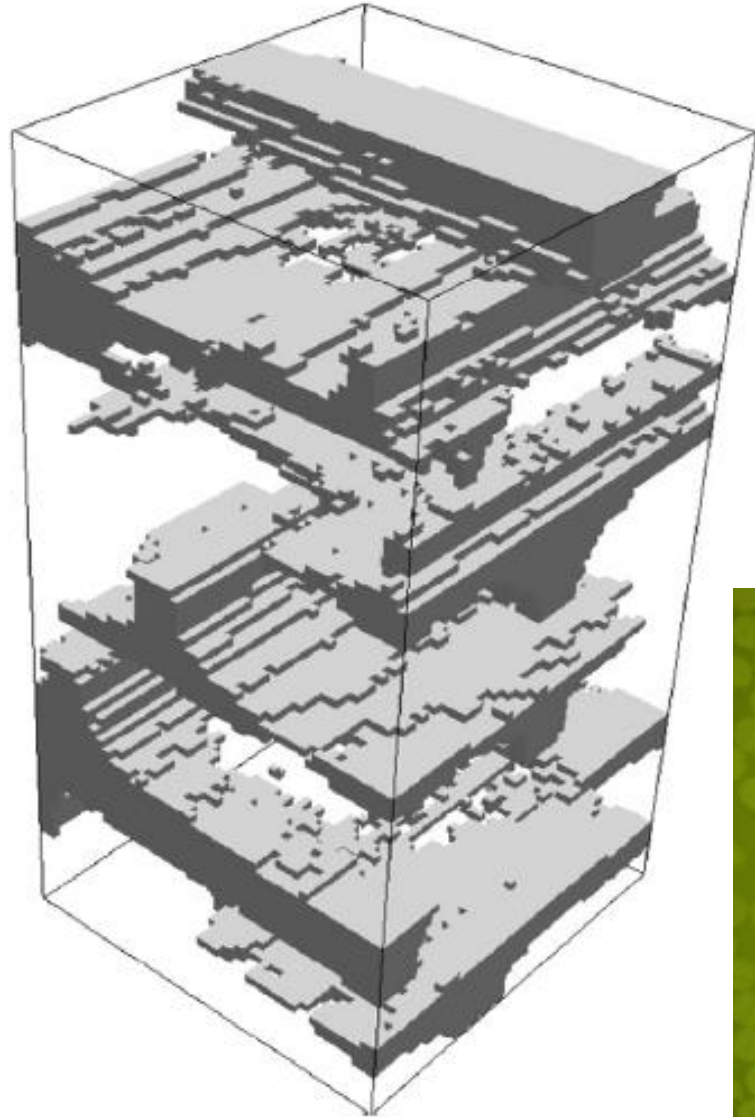
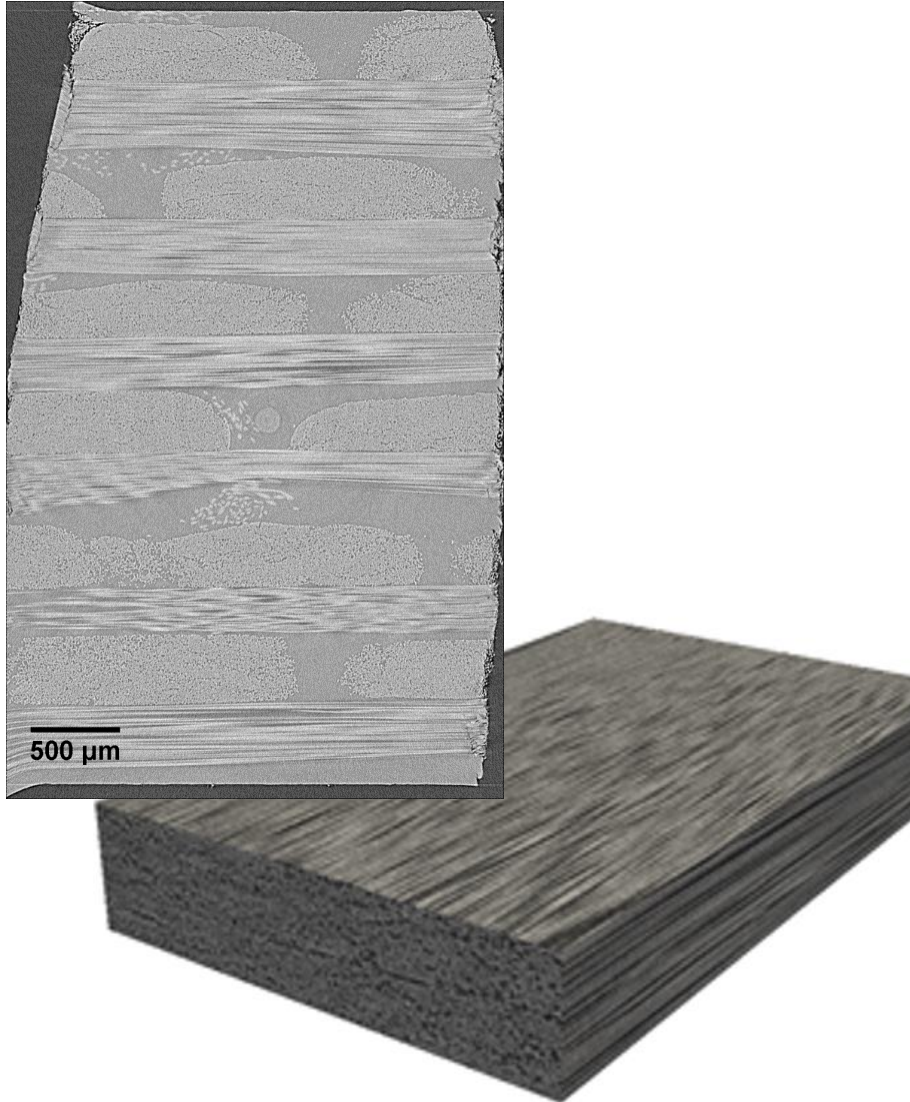


3D woven glass fibre textile

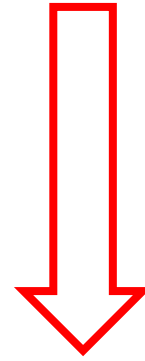


random steel fibre assembly

Textiles: Dual scale



yarn,
bundle &
pore size
~100 μm



fibre & pore
size ~10 μm



1. Introduction. Fibrous media: microstructural features and characteristics

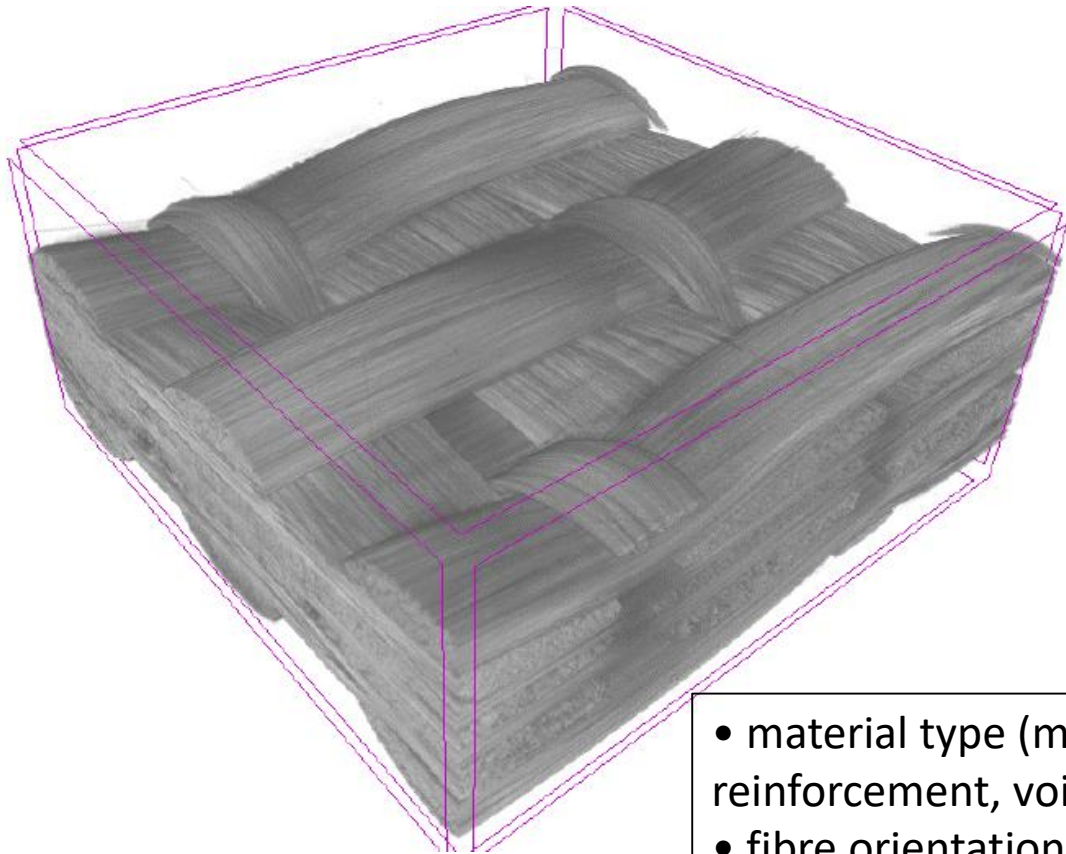
2. Quantification of a μ CT image of fibrous materials

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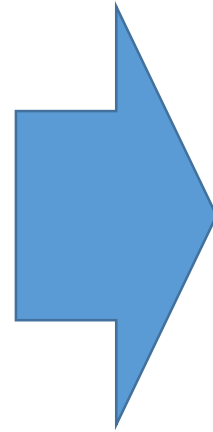
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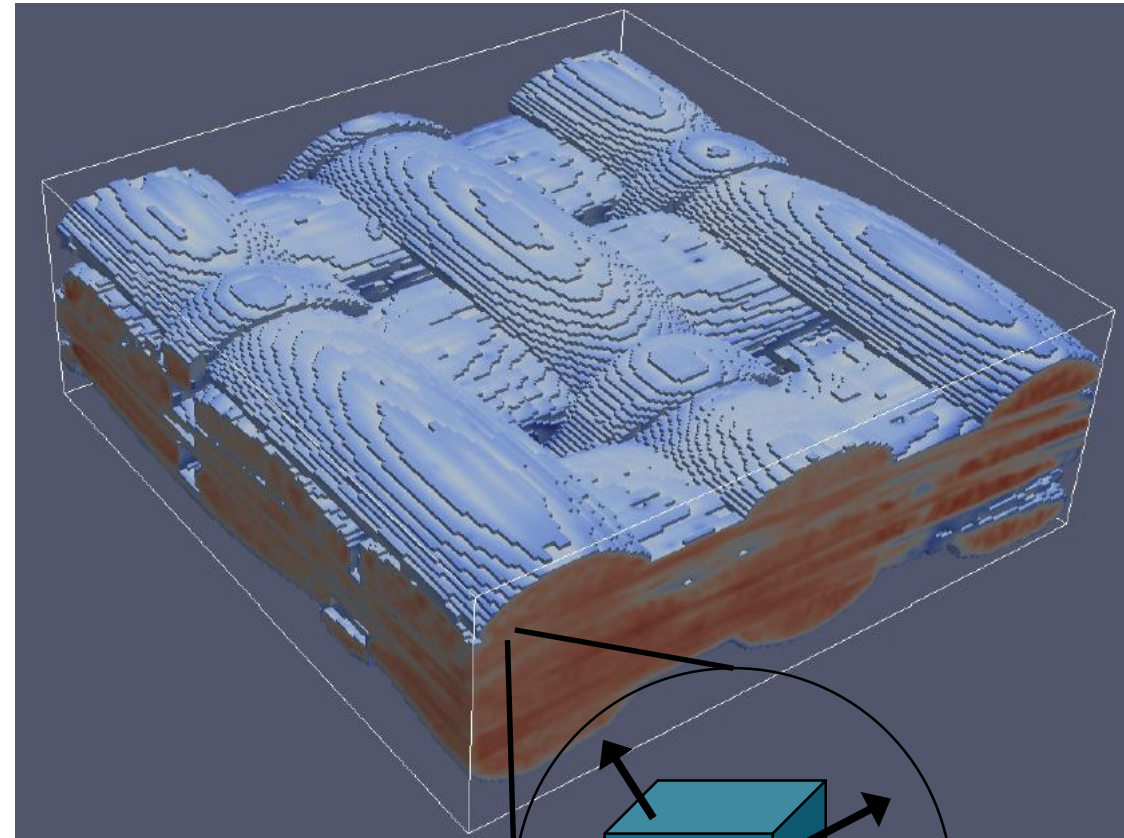
μ CT image \rightarrow voxel model



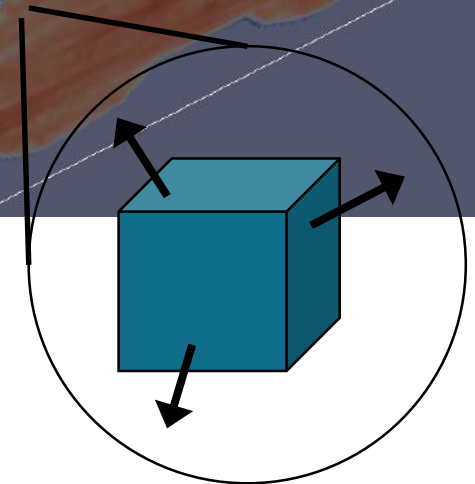
~100 mio pixels



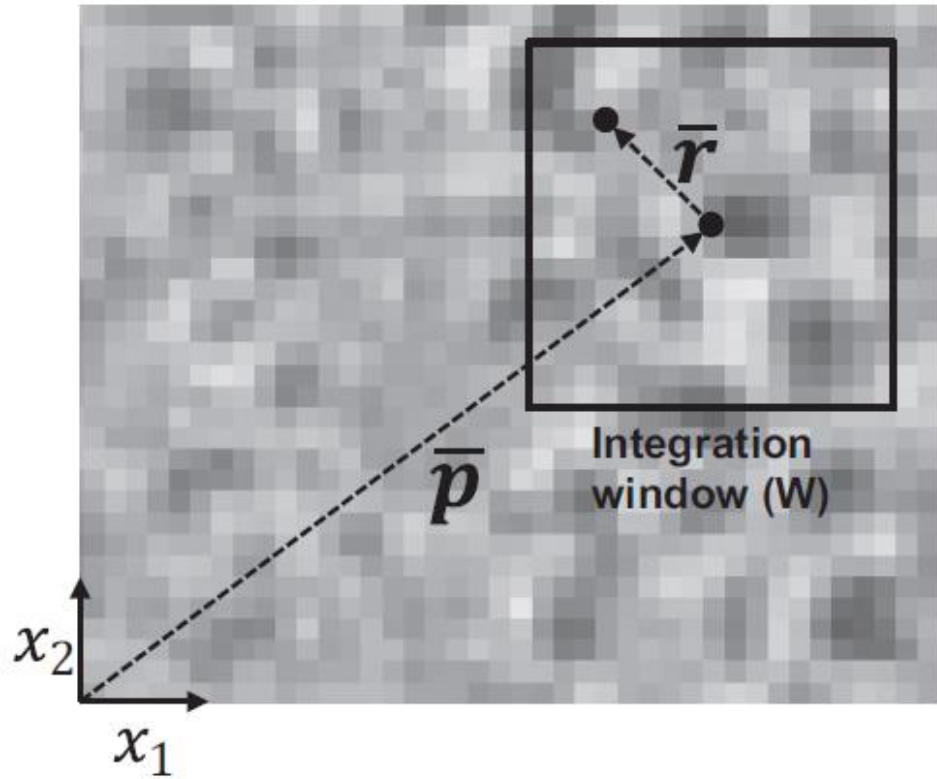
- material type (matrix, reinforcement, void);
- fibre orientation vector (for the reinforcement only);
- local fibre volume fraction (for the reinforcement only).



~500,000 voxels



Structure tensor and anisotropy



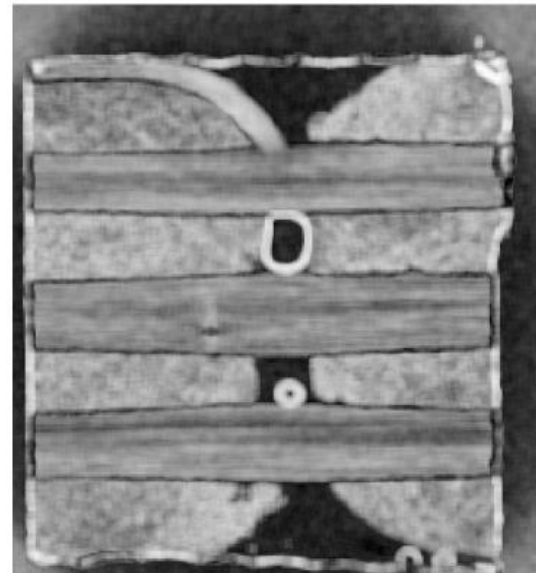
$$S(\mathbf{p}) = \int_{W(\mathbf{p})} S'(\mathbf{r}) d\mathbf{r}$$

$$S'(\mathbf{r}) = \begin{bmatrix} \left(\frac{\partial I}{\partial x_1}\right)^2 & \frac{\partial I}{\partial x_1} \frac{\partial I}{\partial x_2} & \frac{\partial I}{\partial x_1} \frac{\partial I}{\partial x_3} \\ \frac{\partial I}{\partial x_2} \frac{\partial I}{\partial x_1} & \left(\frac{\partial I}{\partial x_2}\right)^2 & \frac{\partial I}{\partial x_2} \frac{\partial I}{\partial x_3} \\ \frac{\partial I}{\partial x_3} \frac{\partial I}{\partial x_1} & \frac{\partial I}{\partial x_3} \frac{\partial I}{\partial x_2} & \left(\frac{\partial I}{\partial x_3}\right)^2 \end{bmatrix}$$

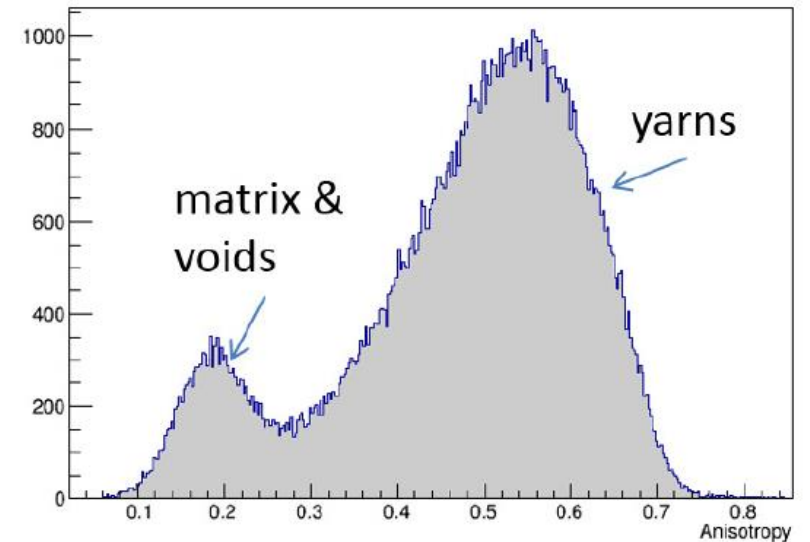
sym

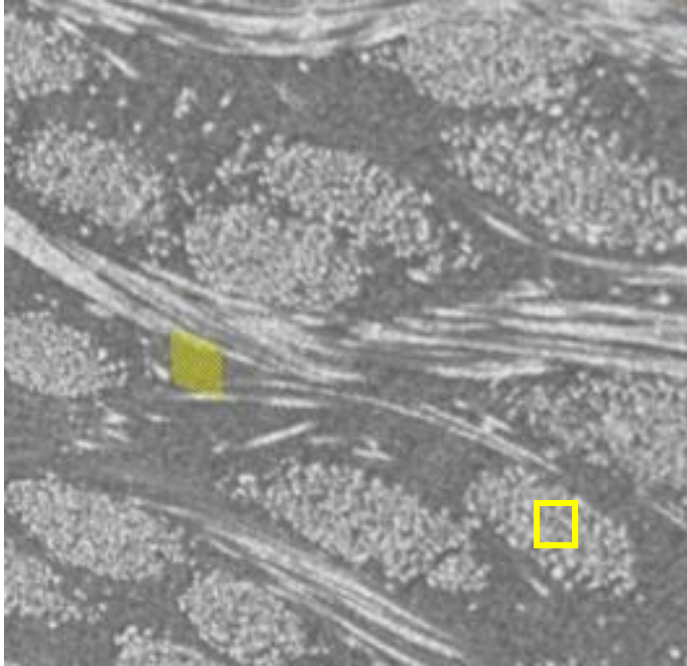
Degree of anisotropy

$$\beta = \begin{cases} 1 - \frac{\lambda_1}{\lambda_3} & \text{if } \lambda_3 > 0, \\ 0 & \text{if } \lambda_3 = 0. \end{cases}$$



3D woven carbon fibre/epoxy composite



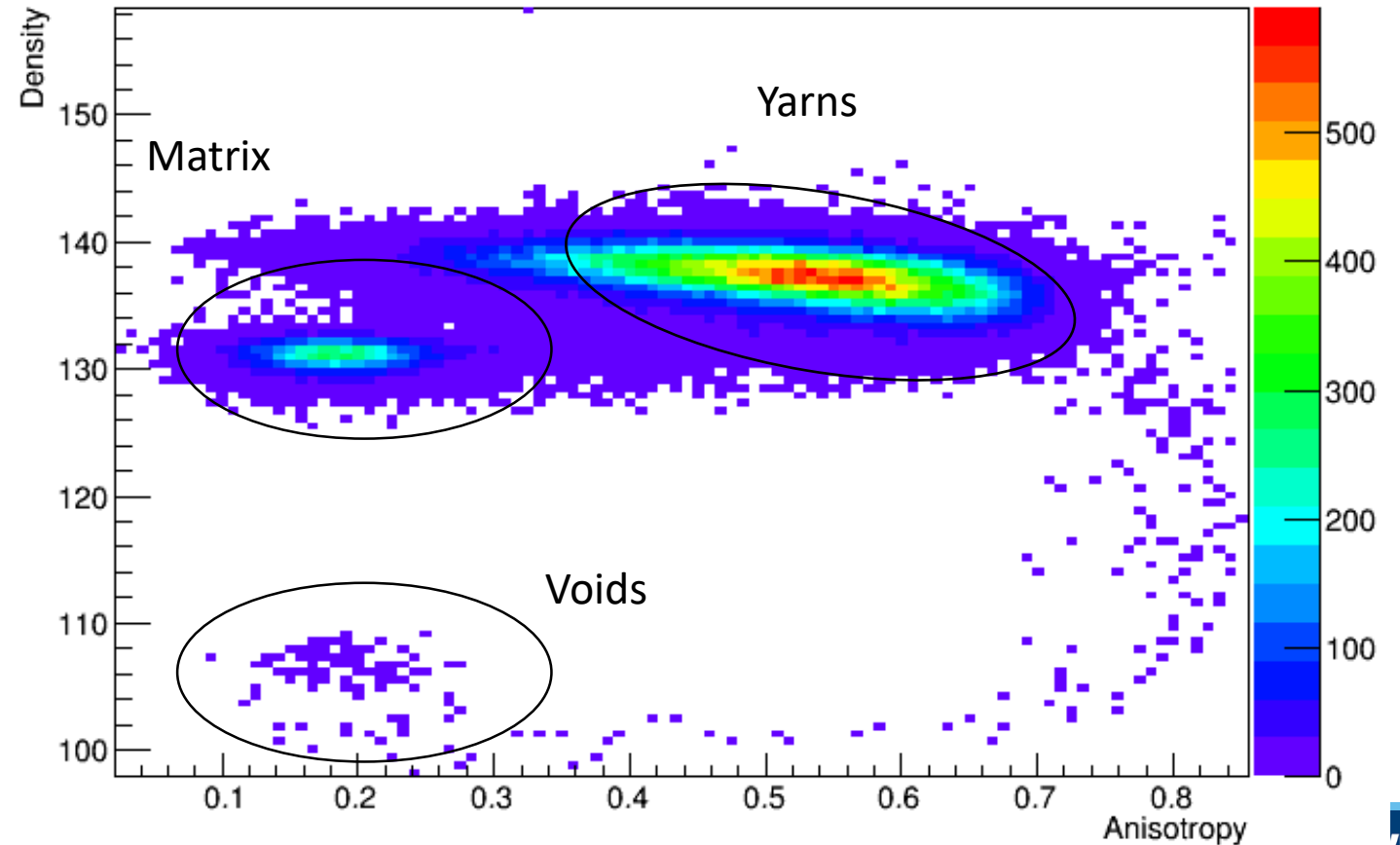


The variables, extracted from the image, reflect physical properties of the material:

- grey value – material attenuation
- structural anisotropy – material microstructure type

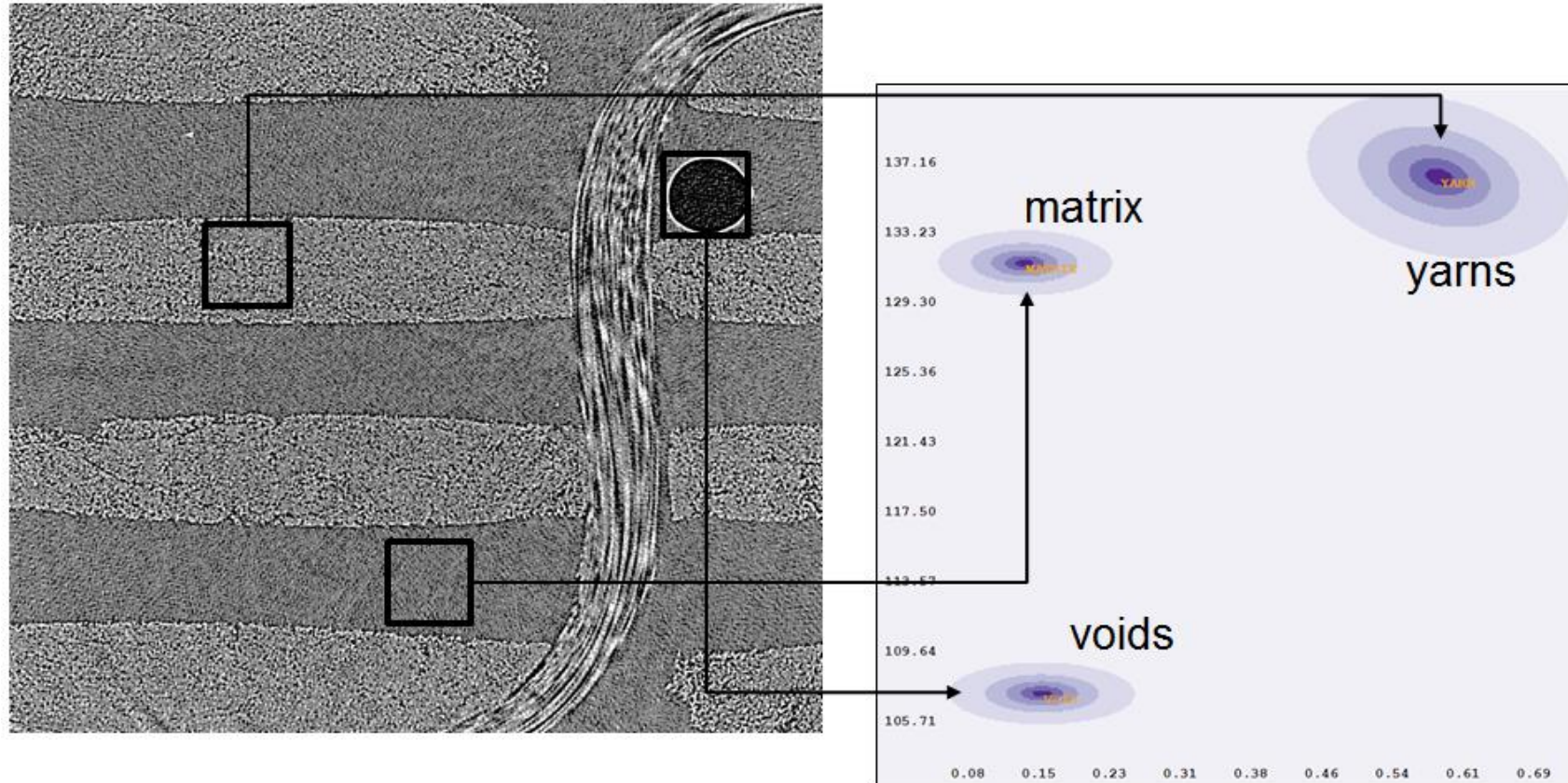
Methods of segmentation:

- Unsupervised (k-means)
- Supervised (Gaussian mixture model)



Supervised segmentation

Uses a training set: selected regions in the image with the class known a priori

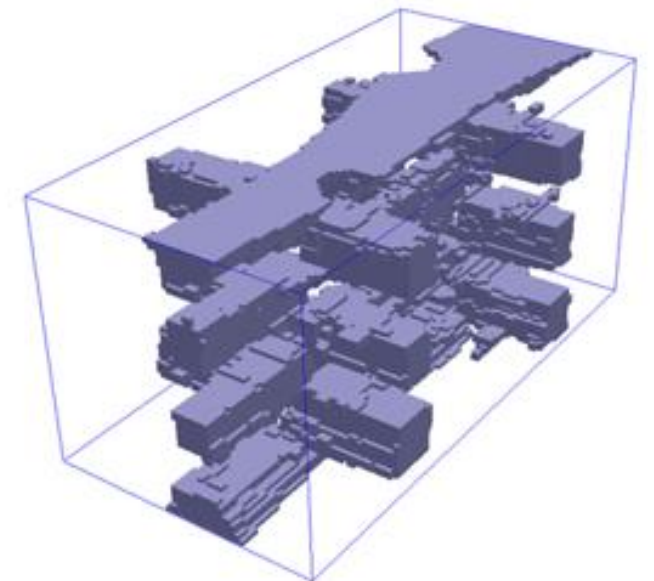


Components defined as Gaussian distributions:

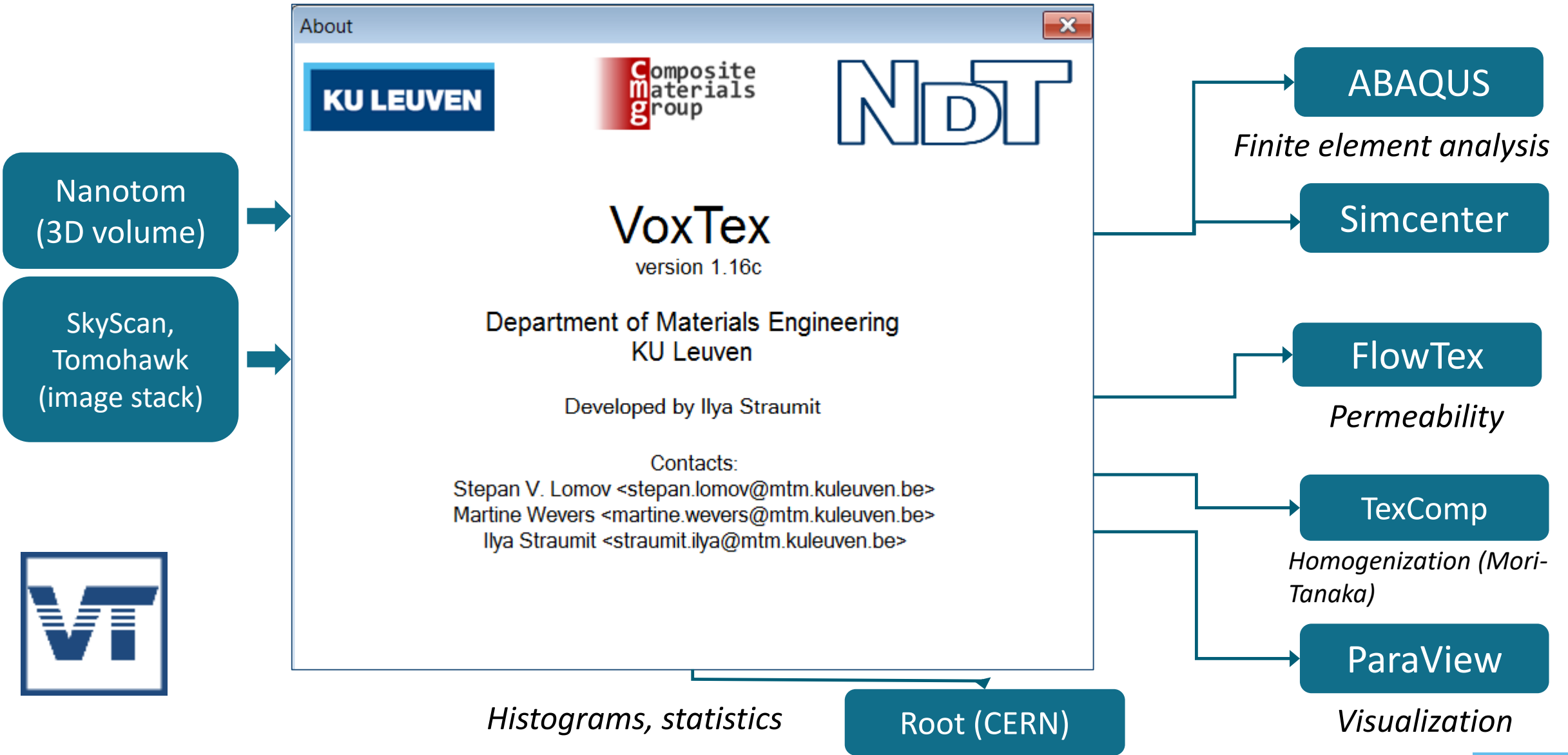
$$L_i(x) = \frac{1}{(2\pi)^{\frac{k}{2}} \sqrt{\Sigma_i}} \exp\left(-\frac{(x - \mu_i)^T \Sigma_i (x - \mu_i)}{2}\right)$$

Classification criterion:

$$C(x) = \operatorname{argmax}_i L_i(x)$$



VoxTex software

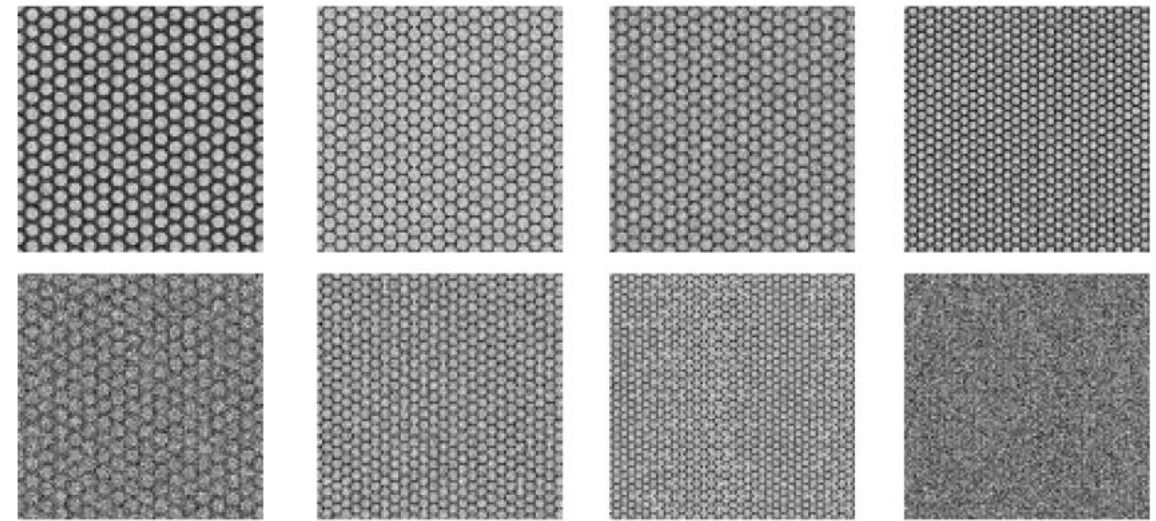
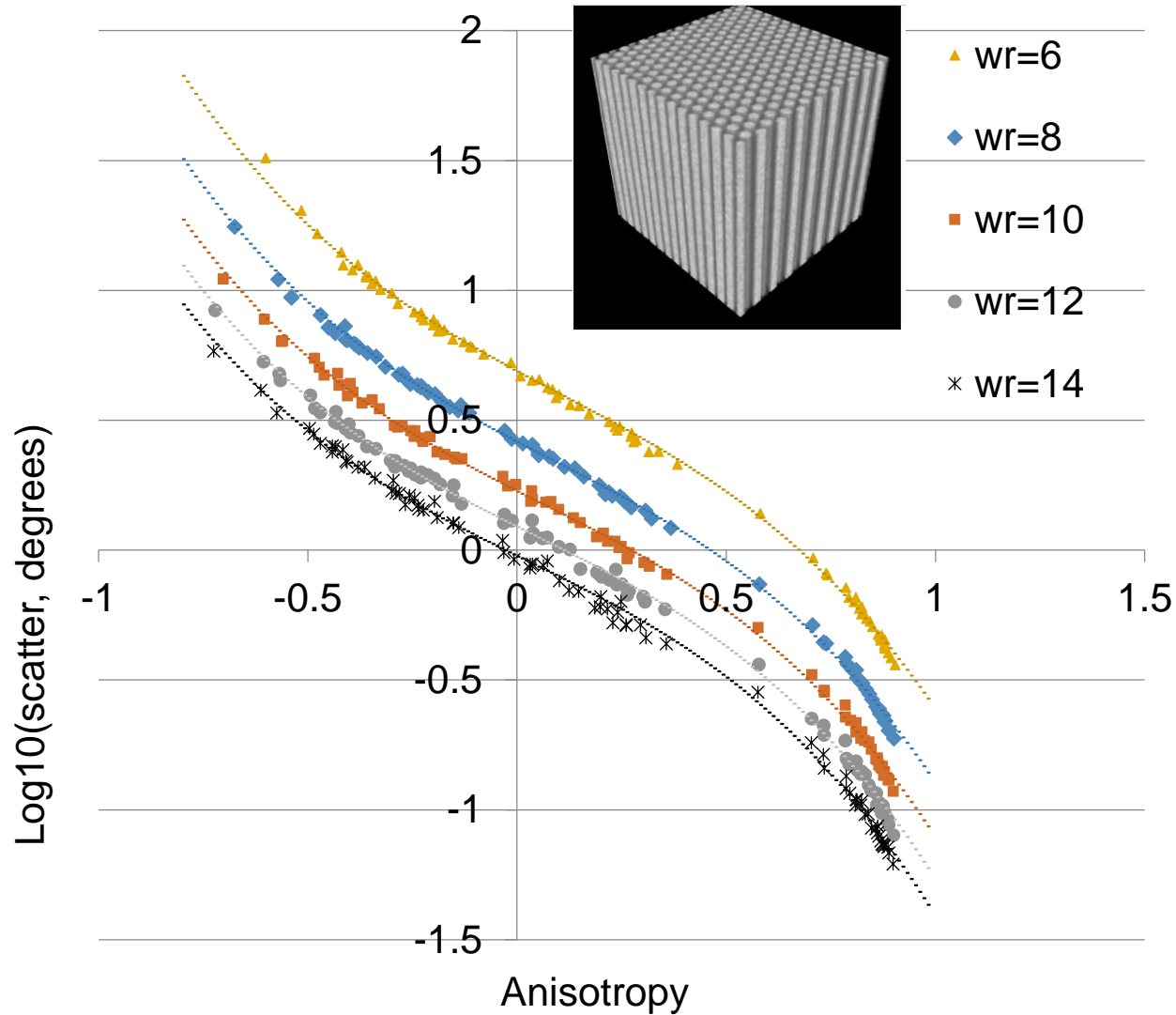


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Estimation of precision and pixel size requirements

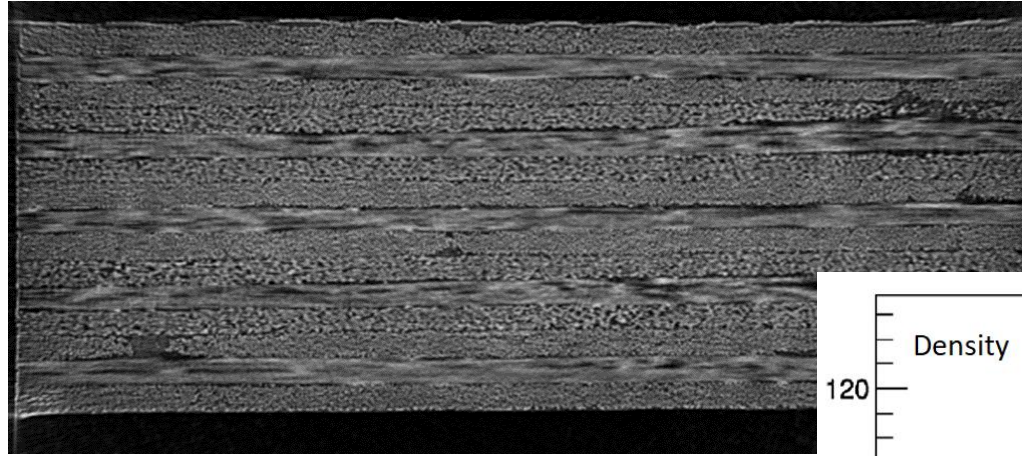


Recommended voxel size parameters

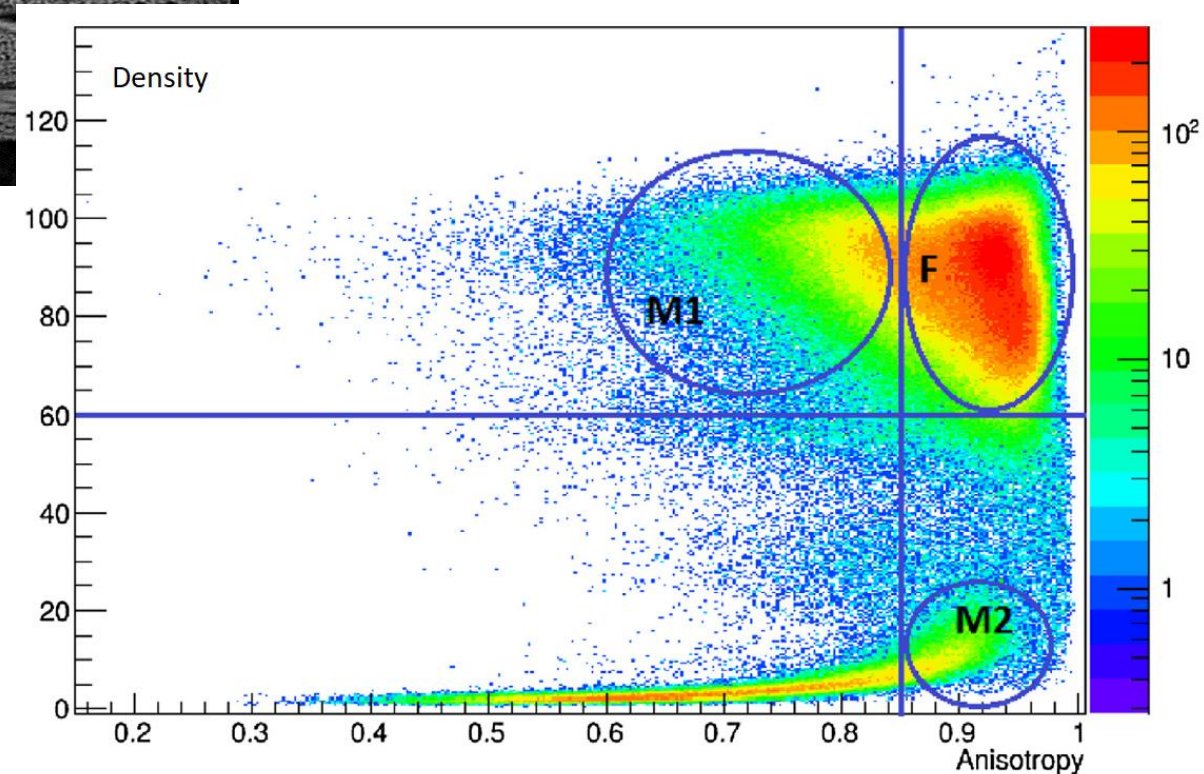
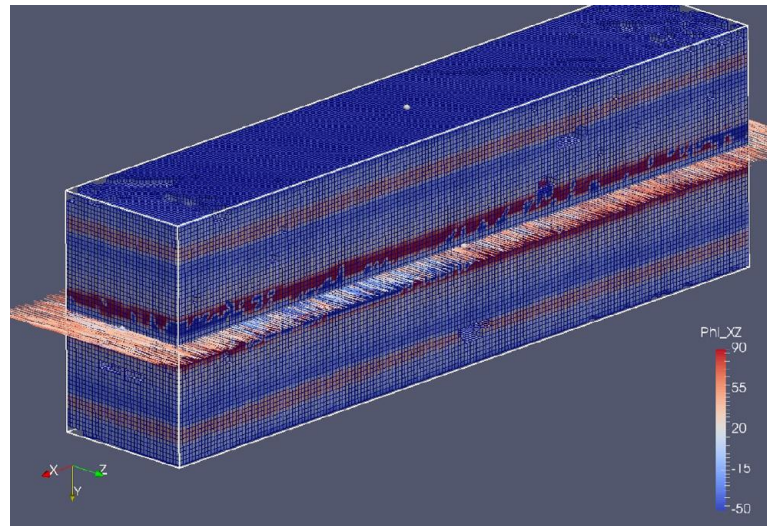
Material	Fibre diameter, μm	Pixel size, μm	Anisotropy	Scatter, degrees
Carbon	7	2.34	0.61	1.1
Flax	15...20	1.48	0.95	0.13
Steel	25	4.4	0.91	0.19
Glass	12	5.5	0.89	0.23

Dry Tape Laying

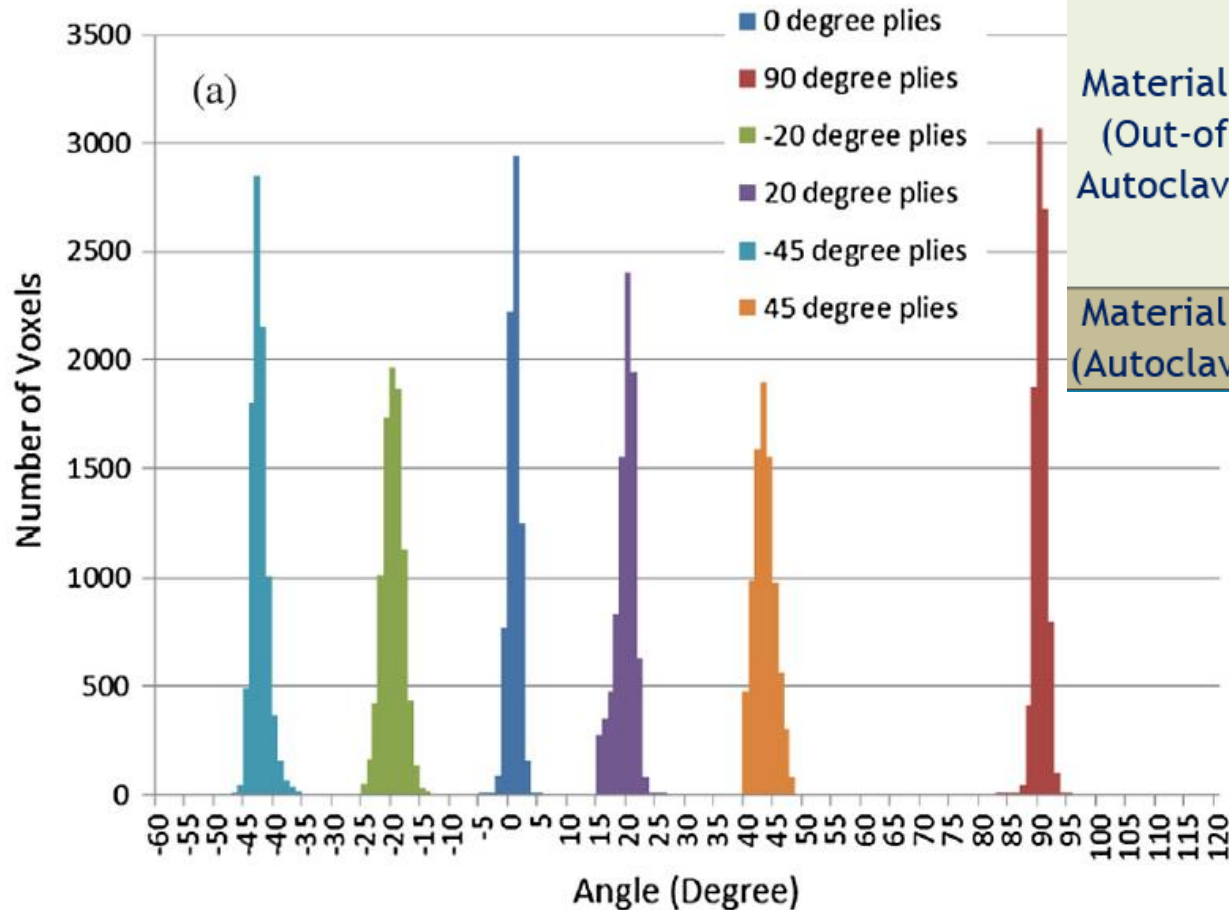
$(-45/0/45/-20/0/20/90/0)_{s_0}$ Produced at NLR, Coriolis machine Hexcel HiTape UD126 - AS7/V800E/QD2/6.35mm



orientations output from the mid-plane of a ply



Fibre orientation: comparison in- and out-of-autoclave

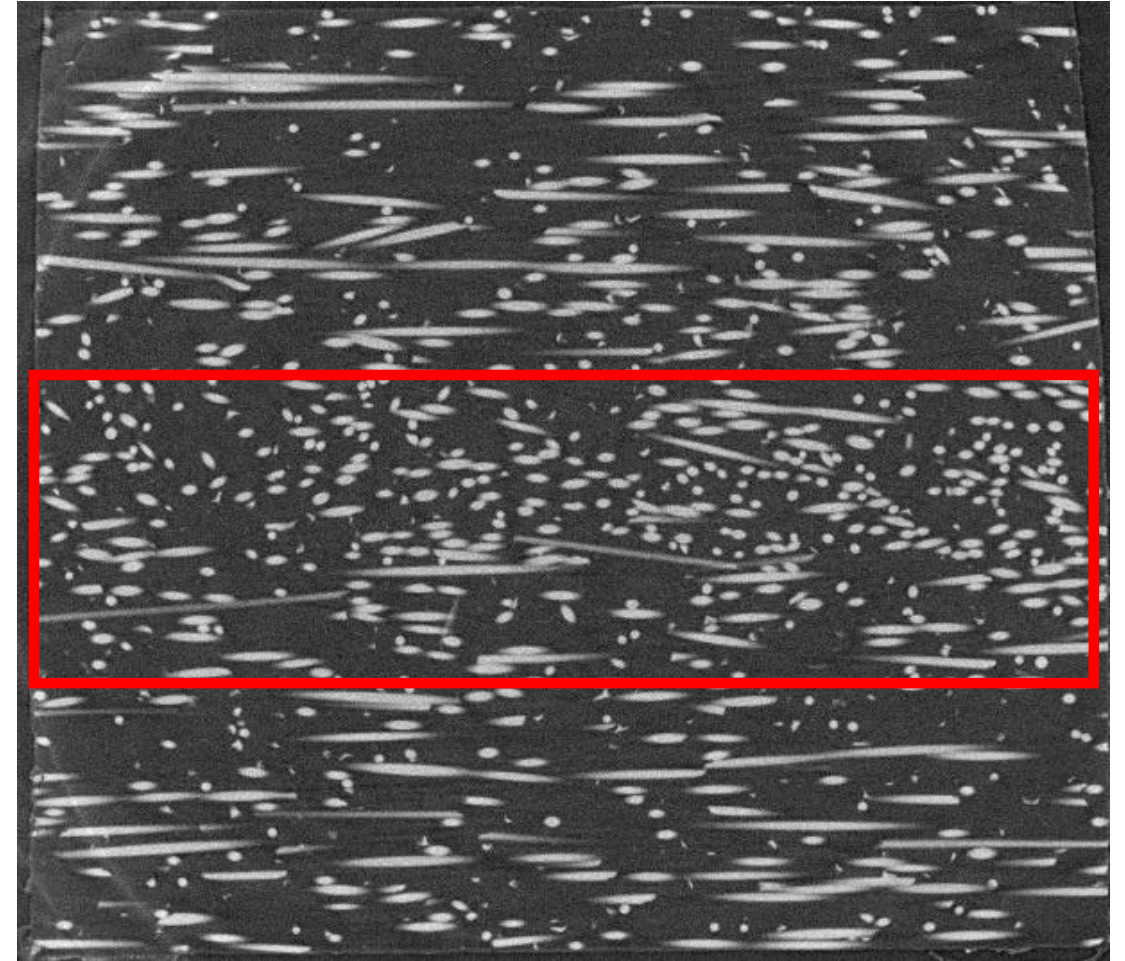
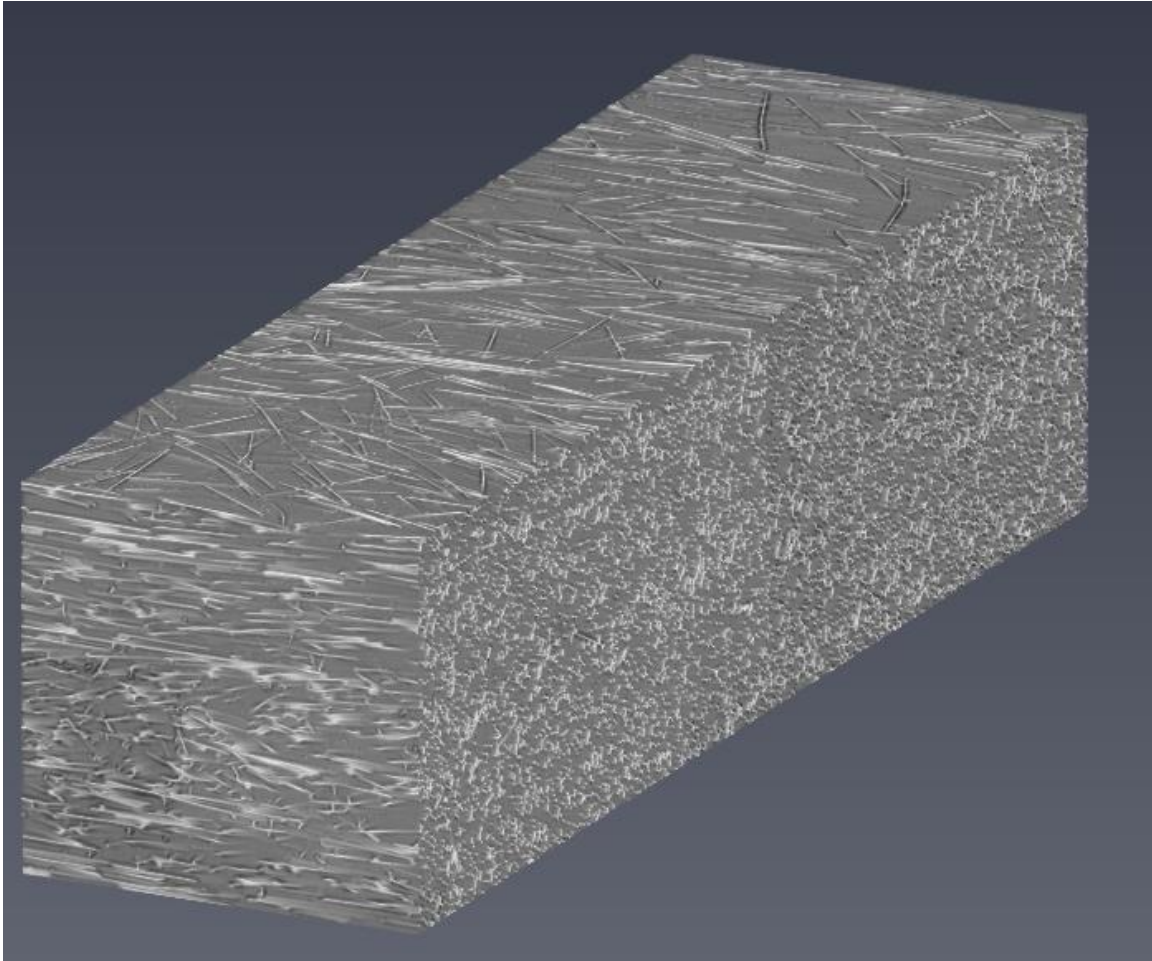


Material Type	In-plane			Out-of-plane
	Nominal Ply Angle α (Degree)	Ply Angle φ_t^α (Degree)	Fibres misalignment m_φ^α (Degree)	Fibres misalignment m_θ^α (Degree)
Material A (Out-of-Autoclave)	0	0.2	1.01	0.79
	20	19.0	1.70	1.34
	-20	-20.5	1.72	1.05
	45	44.0	1.80	2.4
	-45	-43.1	1.42	1.6
	90	90.3	1.11	0.84
Material B (Autoclave)	22.5	23.7	3.80	1.20
	67.5	66.7	2.16	1.25

Material A - automated dry fibre placement and subsequent vacuum-assisted resin transfer moulding
 Material B - automated prepreg tape laying and subsequent autoclave curing

Difference in misalignment because of the high autoclave pressure

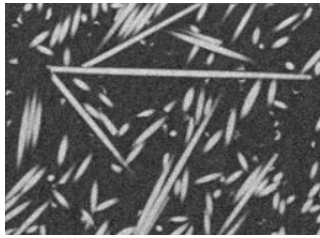
Random short fibre composites: glass/PP



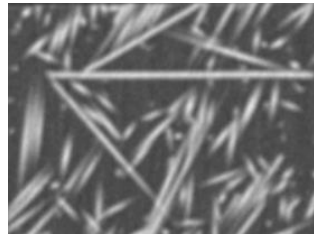
Validation of VoxTex vs ellipsometry (high-fidelity)

Glass fibre/PP composite, VF ~20%, d = 15 μm

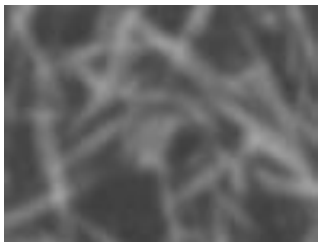
Ellipsometry @ 1.4 μm/pix vs structure tensor @ 16 μm/pix



1.4 μm/pix



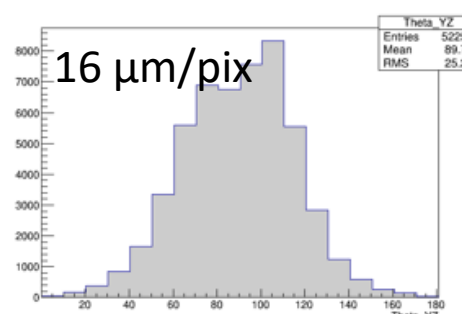
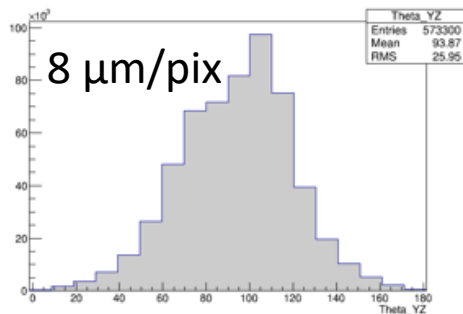
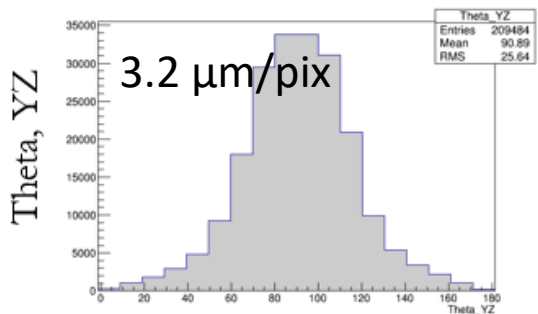
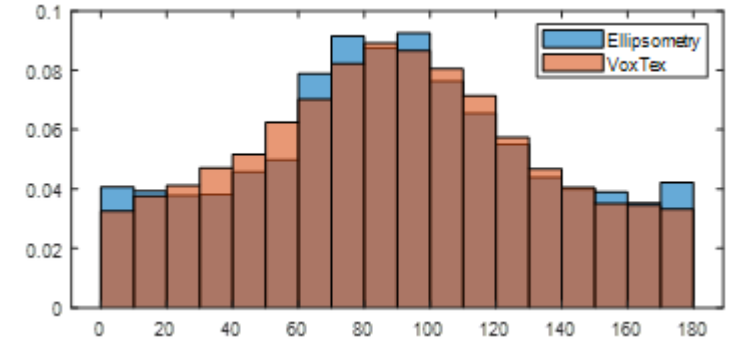
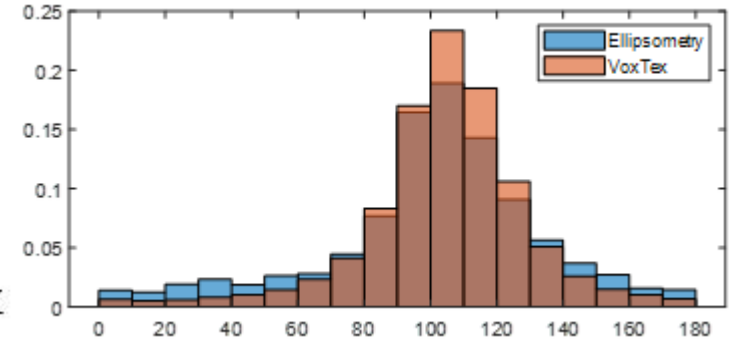
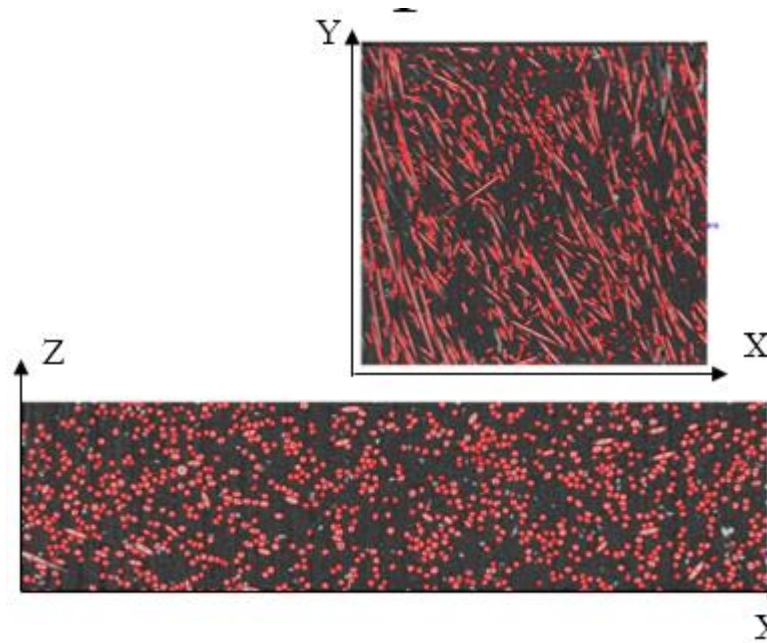
3.2 μm/pix



8 μm/pix



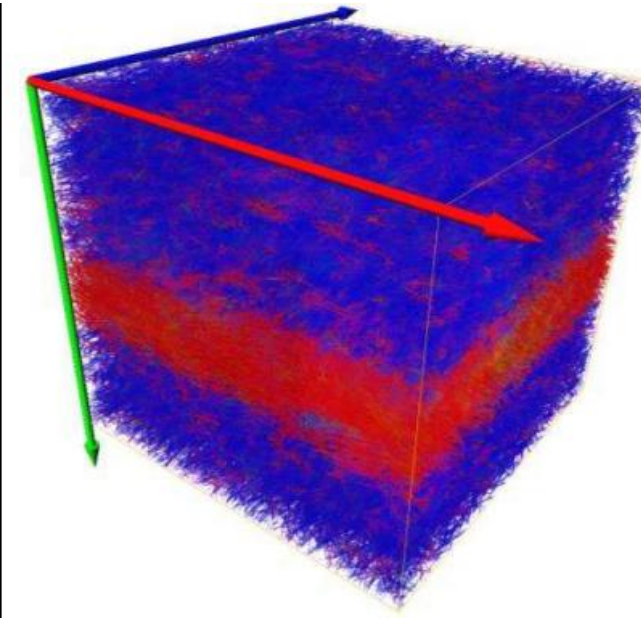
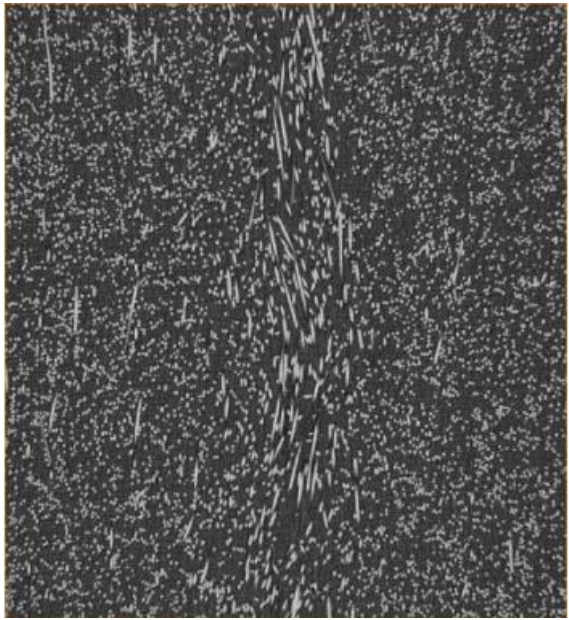
16 μm/pix



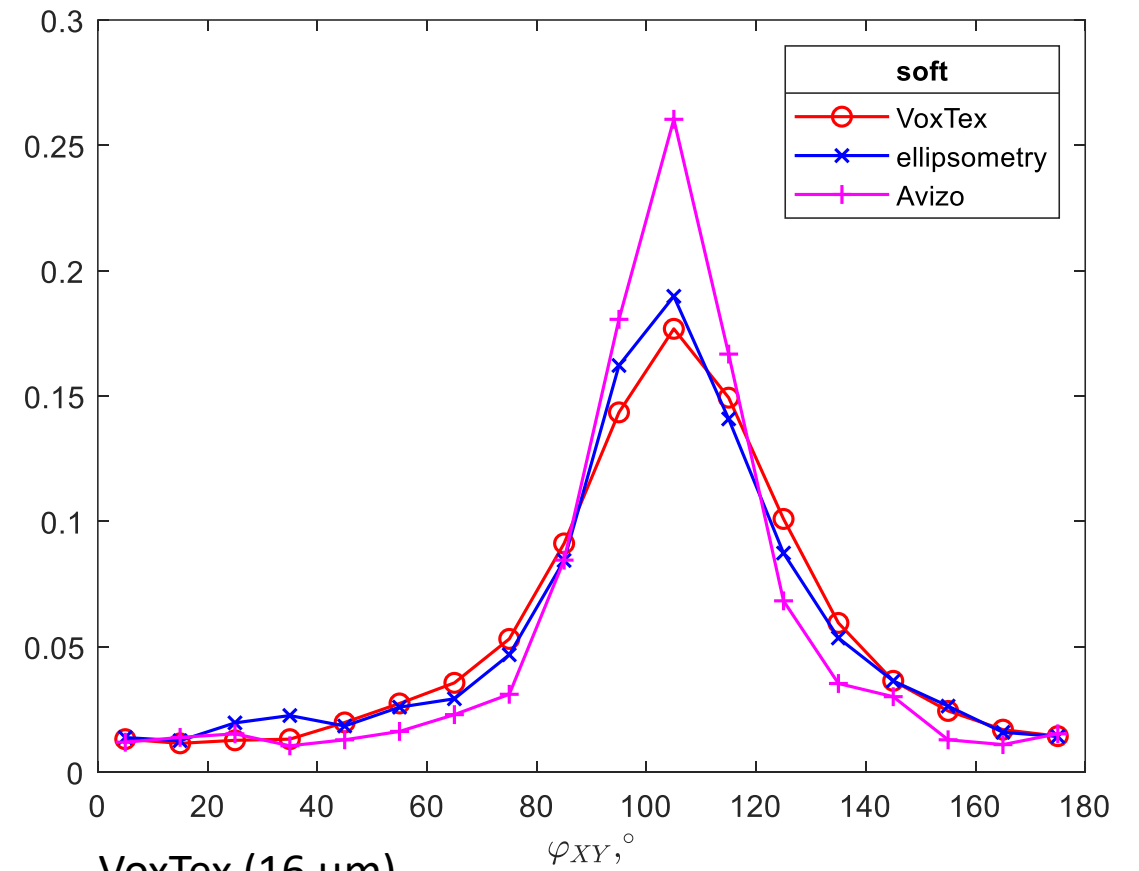
VoxTex, different image resolutions



Validation of VoxTex vs Avizo (high-fidelity)



AVIZO identification of the individual fibres



AVIZO (1.4 μm)

0.199	-0.151	0.006
-0.145	0.739	-0.009
0.006	-0.151	0.061

ellipsometry (1.4 μm)

0.182	-0.145	0.008
-0.145	0.693	-0.081
0.008	-0.081	0.125

VoxTex (16 μm)

0.194	-0.139	0.003
-0.182	0.652	0.02
0.003	0.02	0.154

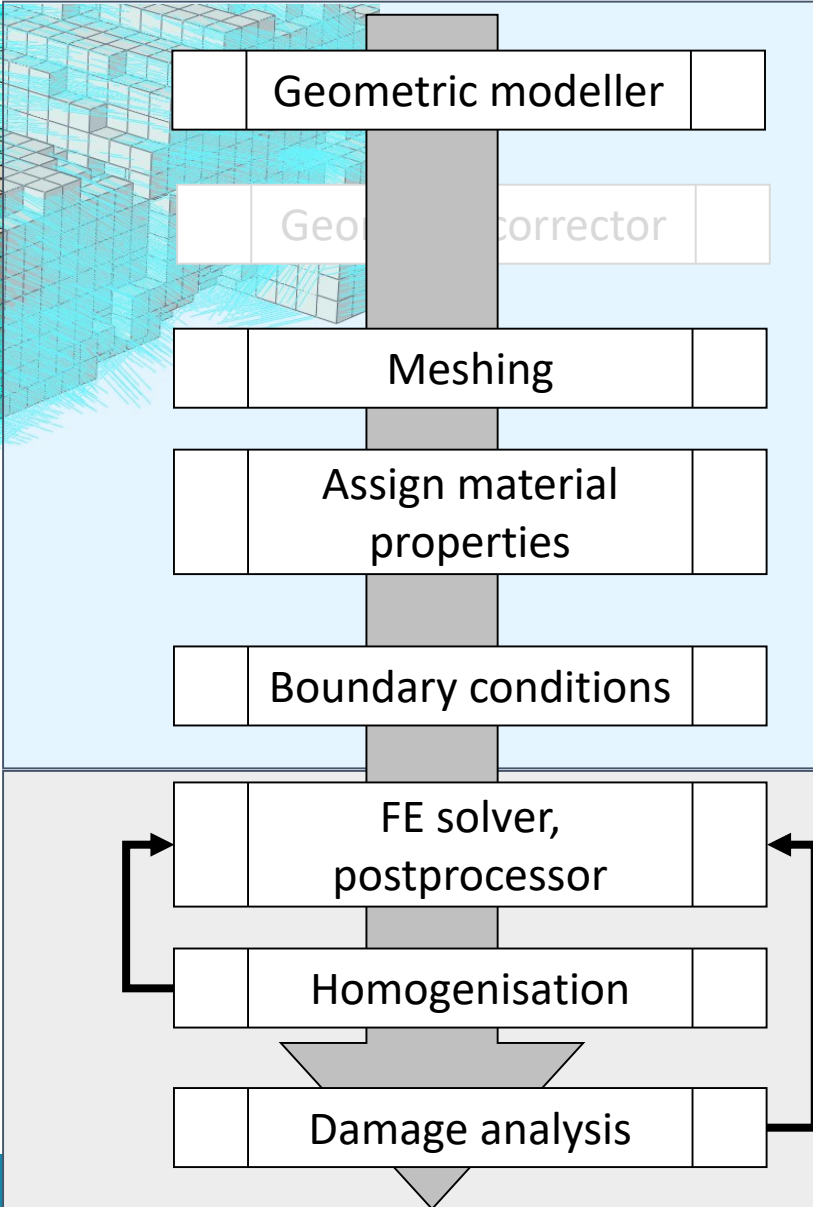
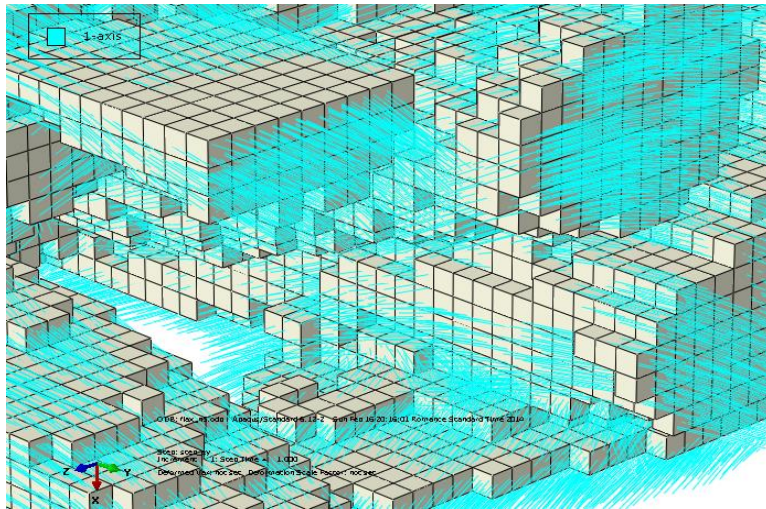


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VoxTex → finite element voxel models



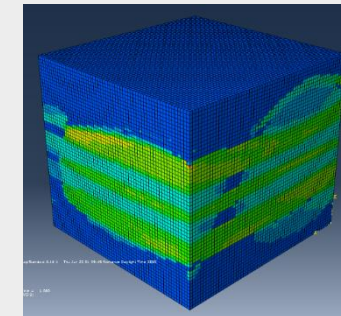
VoxTex creates a voxel model;
after segmentation: identification of materials per voxel

no need for the geometrical corrections

HEX elements = voxels

fibre direction identification (structure tensor) and Chamis UD homogenisation

periodic boundary conditions
NB: “weak” periodicity



**Abaqus
Simcenter**

Impregnated fibre bundle test

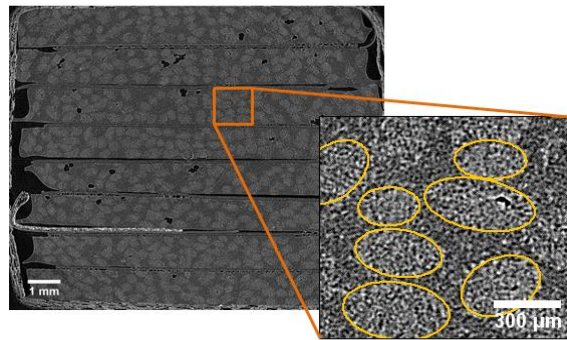
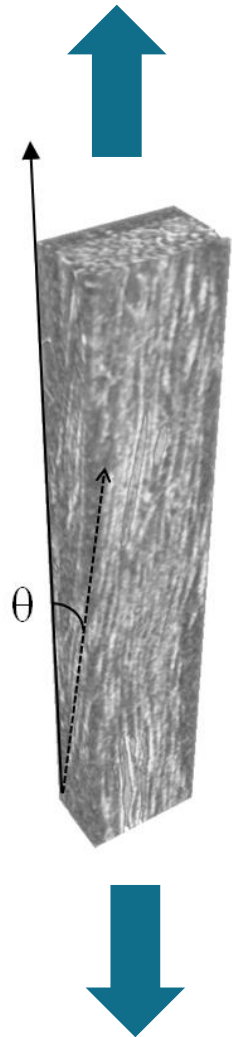
$$E_f = \frac{E_{UD} - E_m(1 - v_f)}{v_f}$$

Quasi-UD flax:
22.9±0.5 GPa -> flax **53.2 GPa**

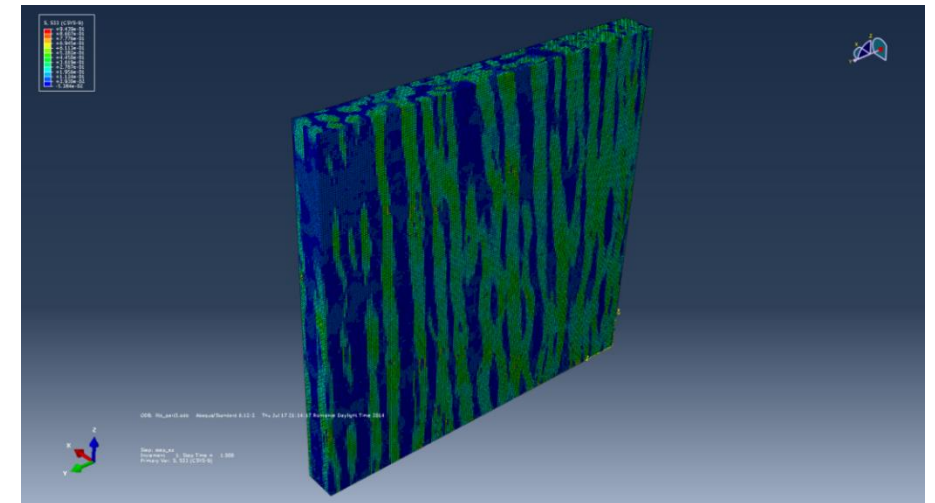
UD flax:
26.6±2.3 GPa -> flax **62.4 GPa**

VF = 40%

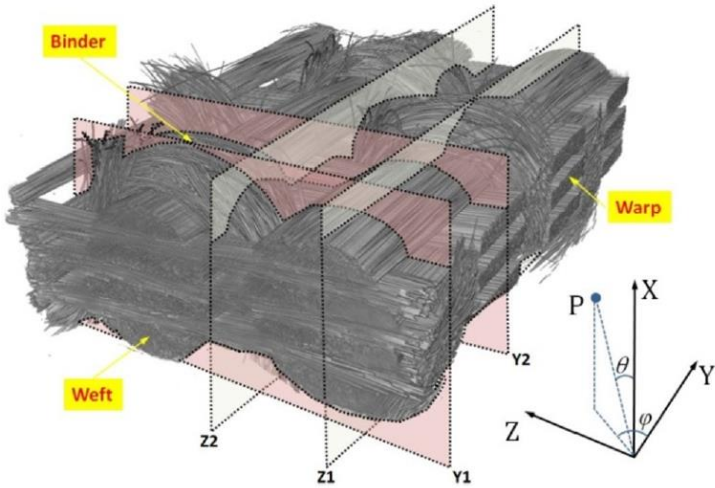
How to obtain correct flax fibre modulus from quasi-UD tests?



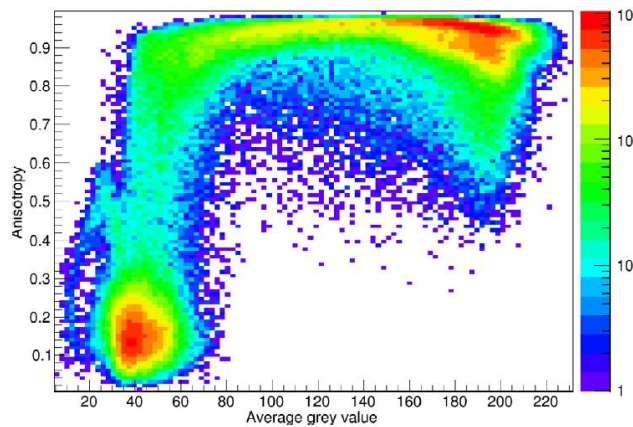
	Fibre volume fraction	Homogenised quasi-UD modulus from FE calculations		Fibre modulus, GPa
		with E _f = 58 GPa	with E _f = 85 GPa	
Sample #1	0.39	21.20	29.27	62.11
Sample #2	0.33	18.36	25.22	62.59
Sample #3	0.31	17.14	23.40	64.19
Sample #4	0.36	19.26	26.34	64.71
Sample #5	0.38	20.88	28.88	61.55
Mean				63.04
Std. Dev.				1.35
CVar				2.1%



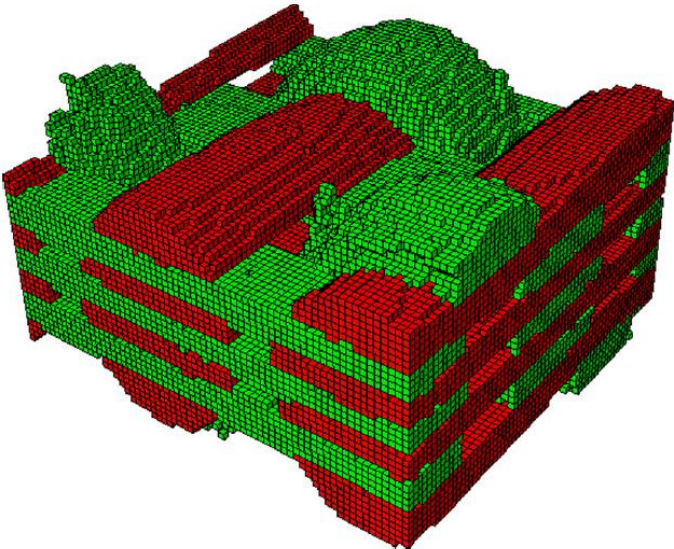
3D woven glass/epoxy composites



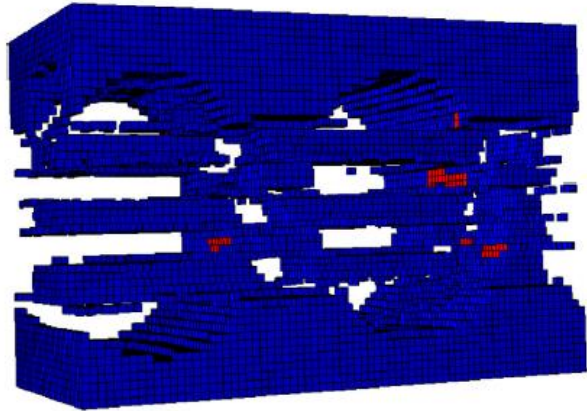
Properties	E-glass Fiber	Epolam 5015 Resin
Tensile modulus E_i^* (GPa)	72	3
Poisson's ratio ν_i	0.3	0.3
Tensile strength X_{iT} (MPa)	2000	80
Compressive strength X_{iC} (MPa)	1350	120
Density (g/cm^3)	2.6	1.1
Yarn linear density (tex)	300	-
Filament diameter (μm)	16	-
Number of fiber per yarn	600	-



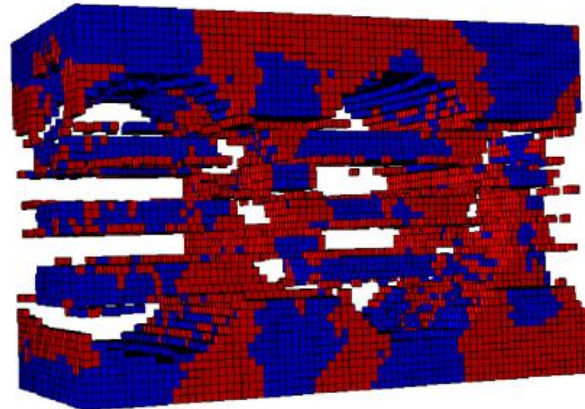
Tensile strength (MPa)	232.6
Tensile ultimate strain	0.0257
Experiment	
Tensile strength (MPa)	$233.8 \pm 1.7\%$
Tensile ultimate strain	$0.0227 \pm 4.6\%$



Damage maps



(a) damage initiation at tensile strain 0.27%

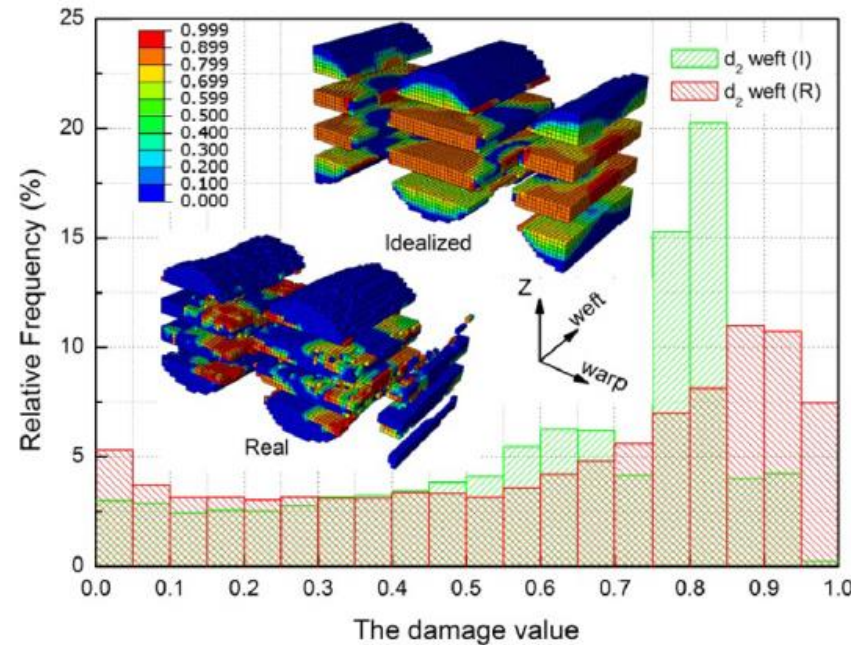


(b) damage evolution at tensile strain 0.68%

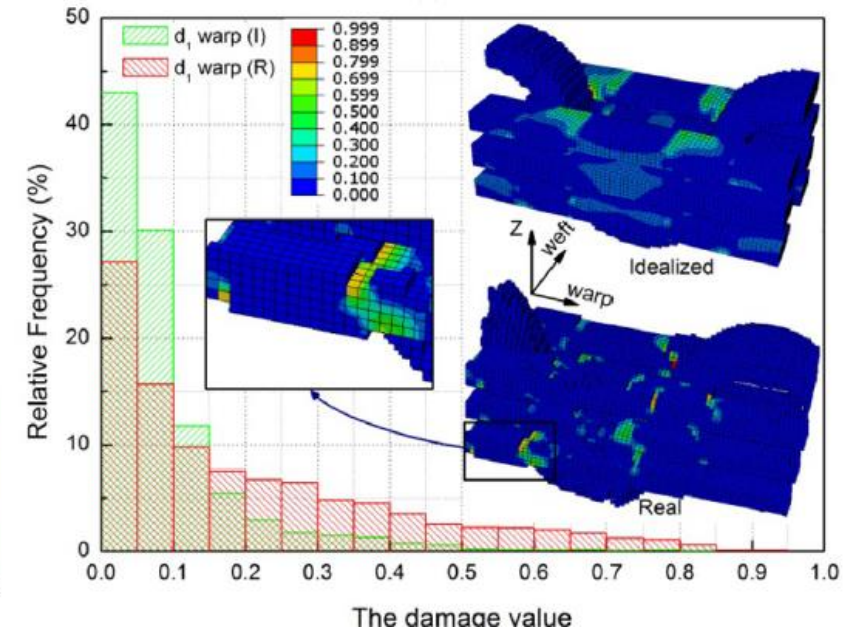
“I” = ideal yarn geometry (TexGen)
 “R” = real yarn geometry (μCT + VoxTex)

damage in the matrix

transverse cracking in the weft



fibre damage

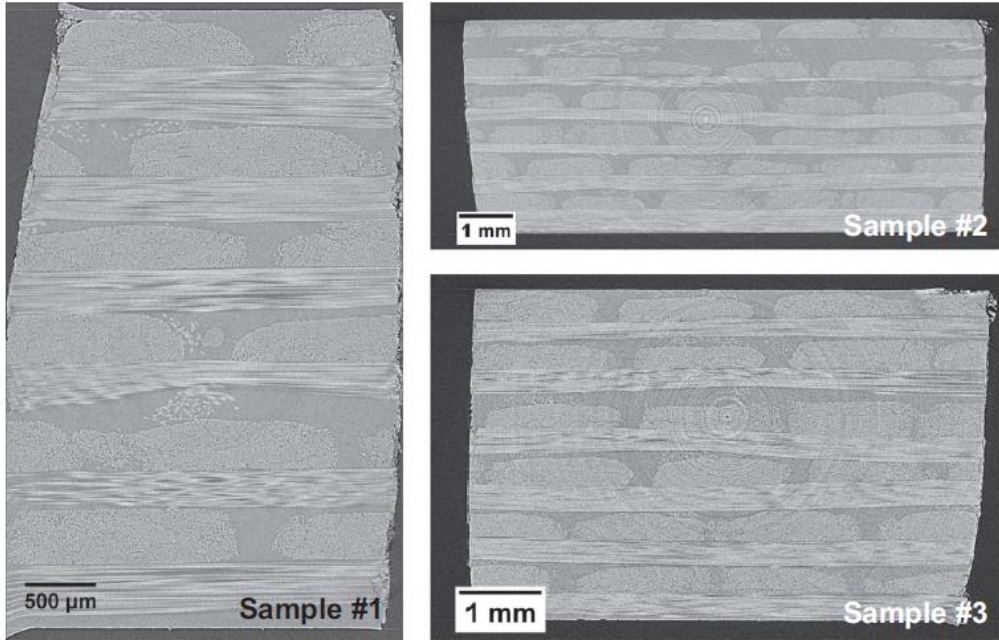


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NCF composites: μ CT images and processing

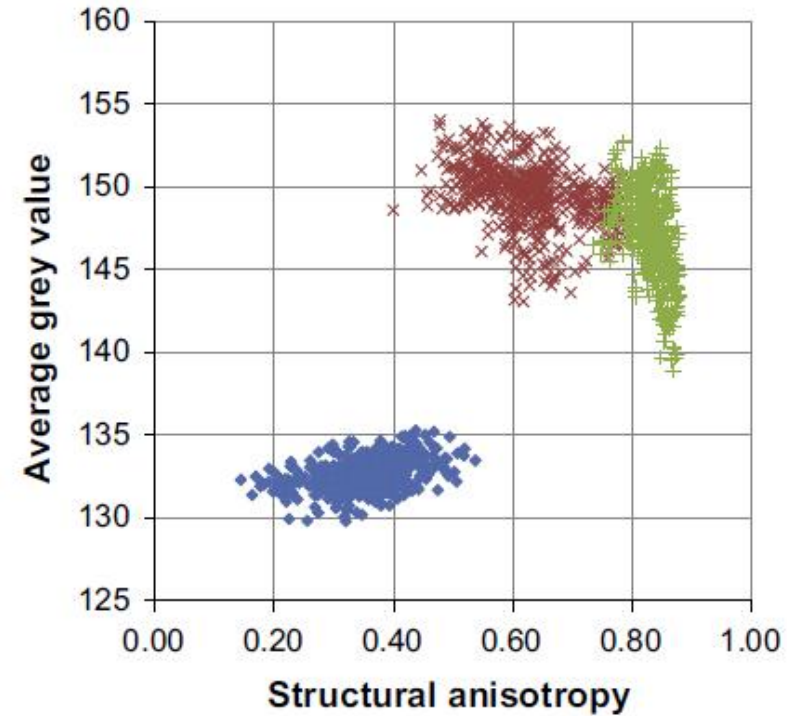
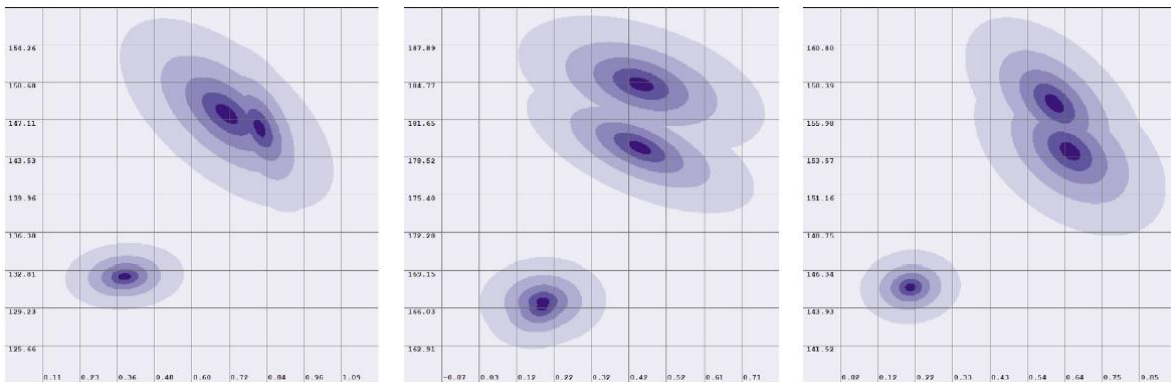


carbon
NCF
(Saertex)
[+45°/-45°]
tricot
stitching,
540 g/m²

sample 1

sample 2

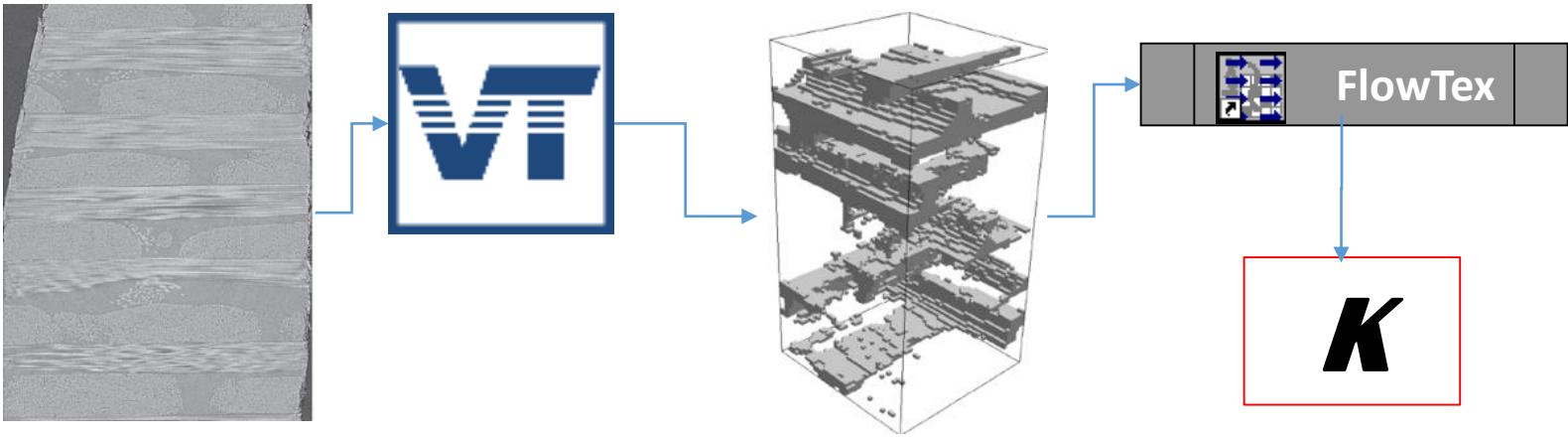
sample 3



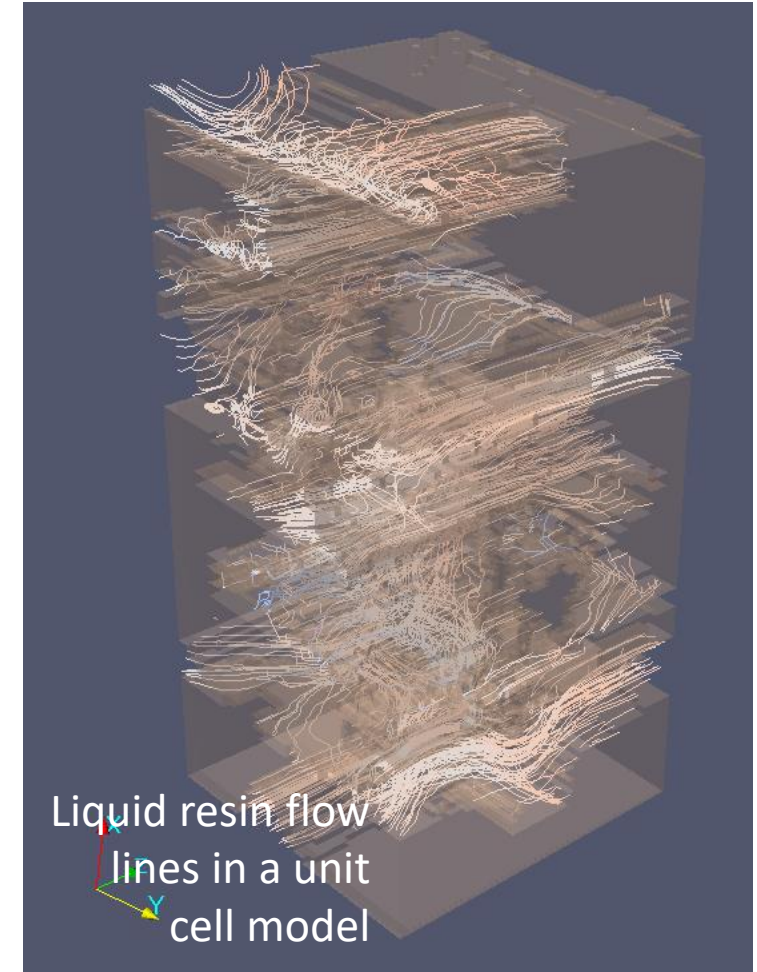
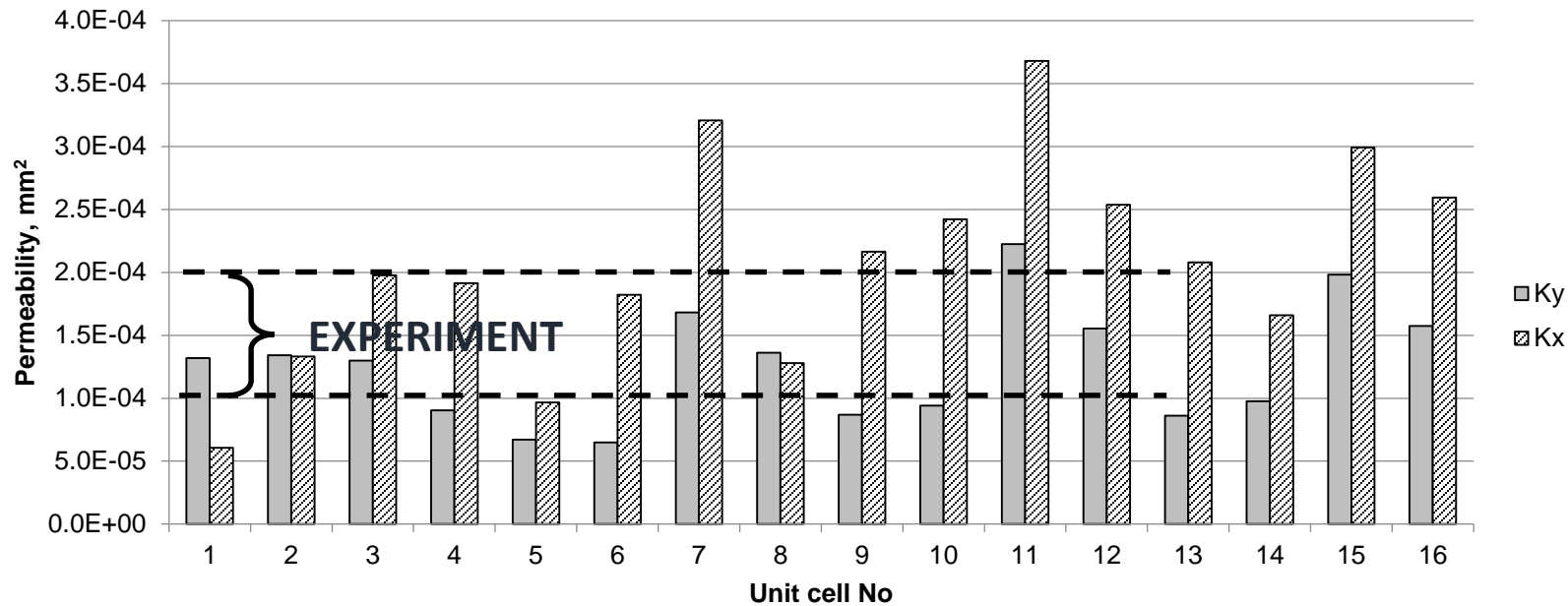
- ◆ Matrix
- × Bundle #1
- + Bundle #2



Permeability calculations



Results for 16 unit cells, resolution of the image 6 μm



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Conclusions



1. **Micro-computed X-Ray tomography is a state-of-the-art tool** for detailed investigation of internal structure of fibrous materials.
2. Lab-scale μ CT allows **quantification of the fibrous structure and a seamless transfer of data to mechanical modelling software**, allowing calculation of:
 - homogenised stiffness
 - damage development and strength
 - permeability
 - effect of defects



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industry	4	
university	7	