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Image-based modelling of C/C and CMC: from µCT to FE models

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Laboratoire des Composites Thermostructuraux (LCTS)

- Joint lab between CNRS, U. Bordeaux, Safran and CEA (~ 80 people)
- High-temperature composites for aeronautics, aerospace, defence & energy applications
- Elaboration, characterisation, testing & modelling







Carbon/Carbon composites (C/C)

- Aerospace applications (T up to 2000°C)
- Carbon fibres and pyrocarbon matrix
- Multilayer architecture + needle punching











Ceramic Matrix Composites (CMC)

- Aeronautics applications
- C or SiC fibres and SiC matrix
- Woven preform





Image-based modelling of C/C and CMC



Prediction of the thermo-elastic properties of a 2.5D C/C



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Modelling of a C/C with a non-linear interface model





High-fidelity FE mesoscale models of woven CMC

Prediction of the thermoelastic properties of a 2.5D C/C

Ph.D. of Morgan CHARRON (2017)

2.5D C/C

- Needle-punched 2D woven plies
- Ex-PAN C fibre and CVI pyC matrix; both anisotropic





Data to be derived from μCT

• bulk/porosity segmentation + local fibre orientation



Segmentation of the porosity



Size distribution of open porosity (Hg pycnometry)







• G3D10: gradient filter for fibrous material



C. Mulat, M. Donias, P. Baylou, G. Vignoles, C. Germain, Optimal orientation estimators for detection of cylindrical objects, Signal, Image and Video Processing 2 (1) (2007) 51– 58. doi:10.1007/s11760-007-0035-2.

• Use of the structure tensor

 $G = \nabla I \otimes \nabla I$





XZ-plane

XY-plane

• Influence of the smoothing kernel size W_r





Direction z



Direction y





Apparent bundle properties

- Limited variation of fibre/matrix content between bundles
- Apparent properties from microscale image-based models



• Average properties (transverse isotropic)

 $E_l = 150 \text{ GPa}, E_t = 15 \text{ GPa}$

 $a_l = 1.3 \times 10^{-6} \,^{\circ}\text{C}^{-1}$, $a_t = 4.5 \times 10^{-6} \,^{\circ}\text{C}^{-1}$



Data derived from μCT

• For each voxel : bundle or porosity + local orientation



Full-field simulations for moderate-size model

- Lippman-Schwinger equation for thermo-elasticity
- Iterative solver using FFT





Domain decomposition for larger models

- Decomposition of µCT into sub-volumes
- Computation of apparent properties of each sub-volume (in parallel)
- Effective properties using the coarse mesh



Full-field vs. domain decomposition

FFT FEM sub16 FEM sub32 50 0.5 1e-05 · FFT FEM sub16 FEM sub32 40 0.4 8e-06 6e-06







Comparison with experimental results



Elastic moduli @ 25 °C

(GPa)	Ex	Ey	Ez	G _{xy}	G _{yz}	G _{xz}
Exp.	33	22	-	6	-	-
Num.	32	21	14	7	4	5

Thermal expansion @ 1000 °C

(%)	ex	ey	ez
Exp.	0.28	0.16	0.09
Num.	0.37	0.28	0.21

Modelling of a C/C with a nonlinear interface model

Ph.D. of Amandine RAUDE (2018)

Needle-punched C/C composite

 $\times n$

Х

×n

- Ex-PAN C fiber and CVI pyC matrix
- Needle-punched UD plies (0°/±60°)

0° direction

0°

60°

-60°

Z

Z fibres bundles



Nappe de fibres de carbone





Needle-punched C/C composite

- Lower fibre volume fraction within Z-bundles
- Need to distinguish Z-bundle (needling) from XY-bundle (UD plies)



 $V_f \approx 40 \%$



Introduction of non-linear interface models



• Need to explicitly define interfaces between plies and with Z-bundles

A. P. Gillard, G. Couégnat, S. Chupin, G. L. Vignoles, Modeling of the non-linear mechanical and thermo-mechanical behavior of 3D carbon/carbon composites based on internal interfaces, Carbon 154 (2019) 178–191. doi:10.1016/j.carbon.2019.07.101.

Preliminary model

• Manual labelling on a small volume (4 plies)







Preliminary model

- Conforming tetrahedral mesh from labelled volume
- Initial coarse volume mesh of the bounding box
- Iterative Delaunay refinement with criterion on Hausdorff distance



A side note on CGAL

- CGAL: Computational Geometry Algorithms Library
- C++ library, many packages including multi-domain 3D meshing, tetrahedral remeshing, etc.



https://www.cgal.org/



https://github.com/nschloe/pygalmesh

FE mesh from manual labelling

- Plies (0°/+60°/-60°) + Z-bundles + porosity
- Insertion of interface elements



Interface elements around Z-bundle

• Create masks for each entity by thresholding the local direction



Aiguilletages

Local direction from structure tensor



• Masks for ply bundles (one for each direction)



Interactive Thresholding





Not





Remove Small Spots



Closing



Remove Small Spots





Not



Fill Holes



• Fusion of all the masks + cleaning



• Comparison with manual labelling





Manual labelling



Automated labelling









Comparison with manual labelling



Manual labelling

FE models from automated labelling









Prediction of the thermal expansion

- 5 large FE models extracted from different zones of the material
- Unilateral interface model with friction

XY-direction

• Predictions within the experimental variability (except at 500 °C because of unreliable data for matrix CTE)



Z-direction

High-fidelity FE mesoscale models of woven CMC

Ph.D. of Vincent MAZARS (2018) & Jean BÉNÉZECH (2019)

High-fidelity FE mesoscale models of woven CMC

- Yarns + matrix
- Each yarn must be labelled individually
- Correct topology of the weaving pattern



From idealised models...

• Geometric approach



From idealised models...

• "Mechanistic" approach



... to image-based approaches

- Structure tensor
- Easy to separate weft from warp, but...





• ... hard to separate yarns for one another without prior information



W. Huang, P. Causse, V. Brailovski, H. Hu, and F. Trochu, "Reconstruction of mesostructural material twin models of engineering textiles based on Micro-CT Aided Geometric Modeling," Composites Part A: Applied Science and Manufacturing, vol. 124, p. 105481, Sep 2019.



• Notion of yarns is indeed subjective



Limits of image-based approach

- Yarns need to be reconstructed *a posteriori* to retrieve continuity and correct topology
- Prescribed weaving pattern is not ensured...



C. Chapoullié, J.-P. Da Costa, M. Cataldi, G. L. Vignoles, and C. Germain, "Orientation-guided two-scale approach for the segmentation and quantitative description of woven bundles of fibers from three-dimensional tomographic images," Journal of Electronic Imaging, vol. 24, p. 061113, Nov 2015

Limits of image-based approach

• Practically, incorrect topology and very user-dependent





• Combine image-based approach with a priori geometric model



J. Bénézech, G. Couégnat, Variational segmentation of textile composite preforms from x-ray computed tomography, Composite Structures 230 (2019) 111496. doi:10.1016/j.compstruct.2019.111496.

- Underlying geometric model
- Each yarn is described by its centreline and some cross-sections



J. Bénézech, G. Couégnat, Variational segmentation of textile composite preforms from x-ray computed tomography, Composite Structures 230 (2019) 111496. doi:10.1016/j.compstruct.2019.111496.



• Convergence of the optimisation heuristic

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

Comparison with manual segmentation

μCΤ

manual segmentation

• Image-based model with guaranteed topology

Mesh generation

- Convert geometrical model to "virtual" 3D image
- Easy to correct residual interpenetration or to add matrix
- Quality conformal tetrahedral volume mesh

CMC digital twins

Z

CMC digital twins

Damage simulation in L-shape woven junctions

Damage simulation in L-shape woven junctions

Comparison with in situ tests

V. Mazars, O. Caty, G. Couégnat, A. Bouterf, S. Roux, S. Denneulin, J. Pailhès, G. L. Vignoles, Damage investigation and modeling of 3d woven ceramic matrix composites from x-ray tomography in-situ tensile tests, Acta Materialia 140 (2017) 130–139. doi:10.1016/j.actamat.2017.08.034.
V. Mazars, G. Couégnat, O. Caty, S. Denneulin, G. Vignoles, Multi-scale damage modeling of 3D ceramic matrix composites from in-situ X-ray tensile tests, in: ECCM18, Athens, Greece, 2018, pp. 24 – 28.

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V. Mazars, G. Couégnat, O. Caty, S. Denneulin, G. Vignoles, Multi-scale damage modeling of 3D ceramic matrix composites from in-situ X-ray tensile tests, in: ECCM18, Athens, Greece, 2018, pp. 24 – 28.

Conclusion

Conclusion

- Need for high-fidelity models of complex textile preforms
- Extensive use of structure tensor to detect local fibre direction
- Models with incremental complexity/level of description
- Generation of conforming tetrahedral meshes
- CMC digital twins for multiscale damage simulations

Questions?

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Appendices

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

Initial geometric model with elliptic sections

$$\alpha \gg \beta \gg \gamma$$

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

$$\alpha \approx \beta \gg \gamma$$

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

$$\alpha \approx \beta \approx \gamma$$

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

Best elliptic model with minimal interpenetration

$$\alpha \approx \beta \approx \gamma$$

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

Switched to polygonal sections

$$\alpha \approx \beta \gg \gamma$$

$$E = \alpha E_g + \beta E_d - \gamma (E_p + E_i)$$

Best model with polygonal sections

$$\alpha \approx \beta \approx \gamma$$

Multiscale damage modelling framework

• Virtual tests at micro-scale

Multiscale damage modelling framework

• Stochastic micro-meso bridge

Multiscale damage modelling framework

